

# PRELIMINARY STORMWATER POLLUTION PREVENTION PLAN

**Prepared For** 

# **BEACON VIEWS**

City of Beacon, New York

August 27, 2019

Applicant Information:

Beacon Views, LLC 500 River Avenue Wakefield, New Jersey 08701



Note: This report in conjunction with the project plans make up the complete Preliminary Stormwater Pollution Prevention Plan.

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## 1.0 INTRODUCTION

#### 1.1 Project Description

The proposed project is located off of Conklin Street in the City of Beacon. The site is approximately 8.6 acres and is identified as Tax Map No. 6055-03-331123. The parcel is located in the RD-5 zoning district. The subject parcel and surroundings are shown on Figure 1. The project proposes nine (9) multi-family townhouse buildings and associated appurtenances. The primary access to the site will be off Hastings Drive, through the adjoining the former St. Francis Hospital property. An emergency access drive will be provided to the north, through the adjacent parcel. It is proposed to capture and treat the stormwater runoff associated with the proposed improvements.

#### 1.2 Existing Stormwater Runoff Conditions

The subject project is located on one tax parcel off of Conklin Street, immediately north of Hastings Drive. The existing ground cover on the site is characterized as a mixture of woods and open grassed meadow areas. The property generally drains from north to south down to the onsite wetland.

The hydrologic soils groups for the project consists of C/D soils. The designations of the onsite soils located within the proposed limits of disturbance consist of Bernardston Silt Loam (BeB), Canandigua Silt Loam (Ca), and Nassau-Cardigan Complex (NwC) as identified on the Soil Conservation Service Web Soil Survey. The soils boundaries are shown on Figure 2 and 3 of this report.

As previously stated, the stormwater runoff from the existing property generally drains from north to south towards the existing onsite wetland. Approximately 20 acres of offsite stormwater runoff is conveyed through the subject property from offsite runoff. The analysis included in the project SWPPP utilizes one design line, within the onsite wetland, to assess the stormwater runoff from the property and any potential impacts from development to the existing natural resources on the property. The Pre-Development Drainage Map (Figure 2 of this report) shows the location of Design Line 1. The contributing area to Design Point 1 is identified as subcatchment PRE.

#### 1.3 Proposed Stormwater Runoff Conditions

As previously stated, the proposed application includes the construction of nine (9) multi-family town house buildings, asphalt driveway, parking areas and associated appurtenances. Stormwater mitigation for the newly created impervious surfaces will be provided in the form of proposed stormwater management practices (SMP's) discussed further in later sections of this report. The proposed SMP's will be designed to capture and treat runoff from the impervious surfaces associated with the proposed buildings, driveway, parking areas and pedestrian walkways.

It is proposed to maintain the existing drainage patterns on the site to the maximum extent practical in the proposed condition to minimize the impact to the existing downstream wetland. Stormwater treatment for the subject project will be accomplished with several different practices including a hydrodynamic separator and extended detention basin for pretreatment, an infiltration basin and subsurface infiltration system. The stormwater management practices have been sized to capture and treat the Water Quality Volume from the developed area.

The stormwater runoff from the proposed development will be captured in a collection system and conveyed to the stormwater management practices. Pretreatment of the stormwater runoff will be provided with a hydrodynamic separator upstream of the proposed subsurface infiltration system and an extended detention basin upstream of the proposed infiltration basin. The extended detention basin has been designed to act as a flow splitter, discharging the water quality volume to the infiltration basin for

treatment, while detaining and bypassing the larger storm events. The contributing area to the extended detention basin and infiltration basin is shown as subcatchment 1.1S. A flow splitter is proposed upstream of the subsurface infiltration system to discharge the water quality volume to the practice for treatment and bypass the larger storm events. Pretreatment for the subsurface infiltration system will be provided by a hydrodynamic separator upstream of the practice and downstream of the flow splitter. The contributing area to the subsurface infiltration system is shown as subcatchment 1.2S. The subcatchments are shown in Figure 3 of this report.

As shown in the following sections of this report, the stormwater quality and quantity for the proposed development have been mitigated to the maximum extent practicable to minimize the impacts to the existing conditions of the downstream, onsite wetland. Additionally, an erosion and sediment control plan has been prepared in accordance with the *New York State Standards and Specifications for Erosion and Sediment Control* to protect the existing waterbodies and drainage features during construction activities and in the post development condition.

#### 2.0 STORMWATER MANAGEMENT

The proposed stormwater management system for the Beacon Views has been designed to meet the requirements of local, city, and state stormwater ordinances and guidelines, including but not limited to those of the City of Beacon and the NYSDEC.

Since the subject project proposes the disturbance of more than one (1) acre, coverage under the New York State Department of Environmental Conservation (NYSDEC) SPDES General Permit No. GP-0-15-002 is required. In order to meet the requirements, set forth by this permit, the latest edition of the NYSDEC *New York State Stormwater Management Design Manual* (NYSSMDM) was referenced for the design of the proposed stormwater management system. The NYSSMDM specifies five design criteria that are discussed in detail below. They are Runoff Reduction Volume, Water Quality Volume, Stream Channel Protection Volume, Overbank Flood Control, and Extreme Flood Control. The first two of the requirements relates to treating water quality, while the later pertain to stormwater quantity (peak flow) attenuation.

To address stormwater quantity requirements of the NYSDEC, the "HydroCAD" Stormwater Modeling System," by HydroCAD Software Solutions LLC in Tamworth, New Hampshire, was used to model and assess the peak stormwater flows for the subject project. HydroCAD is a computer aided design program for modeling the hydrology and hydraulics of stormwater runoff. It is based primarily on hydrology techniques developed by the United States Department of Agriculture, Soil Conservation Service (USDA, SCS) TR-20 method combined with standard hydraulic calculations. For details on the input data for the subcatchments and design storms, please refer to Appendices B and C.

The input requirements for the HydroCAD computer program are as follows:

Subcatchments (contributing watershed/sub-watersheds)

- Design storm rainfall in inches
- CN (runoff curve number) values which are based on soil type and land use/ground cover
- Tc (time of concentration) flow path information
- Watershed Area in Acres

Stormwater Basins

- Surface area at appropriate elevations
- Flood elevation
- Outlet structure information

The precipitation values and intensity duration frequency (IDF) curves for the 1-Year, 10-Year, 100-Year 24-hour design storm events and rainfall distribution curves utilized for this report were obtained from the information provided by Northeast Regional Climate Center (NRCC) and the Natural Resources Conservation Service (NRCS) which is available online at *www.precip.eas.cornell.edu*. The values provided for all design storms analyzed have been listed below.

Design Storm	24-Hour Rainfall
1-Year	2.6"
10-Year	4.7"
100-Year	8.3"

The CN (runoff curve number) values utilized in this report were referenced from the USDA, SCS publication *Urban Hydrology for Small Watersheds*. The following is a summary of the various land uses/ground covers and their associated CN values utilized in this report.

Table 2.0.2 – Project Ground Cover and Associated Curve Numbers (CN)

Land Use/Ground Cover	CN Value
Woods, D Soil	77
Meadow, D Soil	78
>75% Grass Cover, D Soil	80
Impervious Surface	98

## 2.1 NYSDEC Runoff Reduction Volume, RRv

The Runoff Reduction Volume (RR<sub>v</sub>) criterion is intended to replicate pre-development hydrology by maintaining preconstruction infiltration, peak flow runoff, discharge volume, as well as minimizing concentrated stormwater flow. As stated in Chapter 4 of the Design Manual, RR<sub>v</sub> may be treated with standard SMP's with RR<sub>v</sub> capacity sized in accordance with the Chapter 4/6 requirements, or with green infrastructure practices (GIP's) sized in accordance with the requirements set forth in Chapter 5. Runoff reduction is achieved when runoff from a site is captured, directed to a SMP or a GIP, infiltrated to the ground, reused, or removed by evapotranspiration, so it does not contribute to the stormwater discharge from the site. The goal for each site is to reduce the entire WQ<sub>v</sub> (100%) through the implementation of GIP's and standard SMP's with RR<sub>v</sub> capacity. However, if 100% of the WQ<sub>v</sub> cannot be reduced by applying a combination of green infrastructure techniques and standard SMP's with RR<sub>v</sub> capacity. In addition, the designer must provide justification in the SWPPP that evaluates each of the green infrastructure techniques listed in Table 3.2 and identify the specific site limitations that make application of the technique(s) infeasible."

For a calculation of the Initial WQ<sub>v</sub> / RR<sub>v</sub>, the RR<sub>v</sub> minimum, the RR<sub>v</sub> / WQ<sub>v</sub> required, and the RR<sub>v</sub> provided, refer to Appendix A. In calculating the RR<sub>v</sub> minimum, onsite soils belongs to the Hydrologic Soil Groups D. These soil groups have a specific reduction factor of 0.20. The table below summarizes the RR<sub>v</sub> requirements for the site, as calculated in Appendix A. As can be seen in the following table the RR<sub>v</sub> provided exceeds the WQv/RR<sub>v</sub> required:

			WQ <sub>v</sub> RR <sub>v</sub> Required		Percentage of WQ <sub>v</sub> Treated
Drainage Area	Initial WQ <sub>v</sub> / RR <sub>v</sub> (c.f.) <sup>1</sup>	RR <sub>v</sub> Minimum (c.f.)	(Initial WQ <sub>v</sub> / RR <sub>v</sub> minus RR <sub>v</sub> provided through GIP with Area Reduction) (c.f.)	RR <sub>∨</sub> Provided (c.f.)	
1.1S	9,558	1,140	9,558	9,650	101%
1.2S	1,531	193	1,531	1,917	125%

<sup>1</sup> Refer to Appendix A for Initial WQ<sub>v</sub> Calculations

As noted in the table above the project has provided greater than the RR<sub>v</sub> required. By implementing GIP's to the greatest extent practicable, and exceeding the RRy required, the NYSDEC RR<sub>v</sub> requirement has been addressed.

2.2 NYSDEC Water Quality Volume, WQv

The stormwater management practices have been designed in accordance with the Performance Criteria (Chapter 4) of the NYSSMDM. As outlined in Chapter 4, the WQv is the runoff volume produced during the 90% storm. The proposed infiltration practices have been designed to treat the WQv in accordance with the NYSSMDM. The following equation, per Chapter 4, was used to determine the water quality volume for the 90% storm for each of the contributing areas to the treatment practices:

The water quality volume shall be  $WQ_v = (P)(R_v)(A)$ 

Where.

, WQv P	<ul><li>water quality volume (in acre-feet)</li><li>90% Rainfall Event Number</li></ul>
R <sub>v</sub>	= $0.05 + 0.009(I)$ , where I is percent impervious cover
Α	= site area in acres

The stormwater management practices have been designed in accordance with the Performance Criteria (Chapter 4) of the NYSSMDM. As outlined in Chapter 4, the WQv is the runoff volume produced during the 90% storm. The proposed infiltration practices have been designed to treat the WQv in accordance with the NYSSMDM. The equation above, per Chapter 4, was used to determine the water quality volume for the 90% storm for each of the contributing areas to the treatment practices:

Table 2.2.1 - Water	Quality	Volume	Calculation	Summary
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Subcatchment	WQ <sub>v</sub> <sup>1</sup>
	(cf)
1.1S	9,558
1.2S	1,531
 1 1 1 1 1 1 A	

<sup>1</sup> For detailed calculations see Appendix A

There are two infiltration practices (NYSDEC Design I-2 and I-4) proposed as part of the development of the site to meet both the WQv and RRv requirements as well as provide the necessary peak flow attenuation to satisfy the overbank and extreme overbank flood control requirements. The infiltration practices are designed as an offline practice with a flow splitter upstream of the practice. The infiltration practices are sized to treat the WQv from the contributing area. Testing has yet to be performed in the areas of the infiltration practices. As such the infiltration

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rate used in the HydroCAD stormwater modeling of the infiltration practices was kept conservative to an infiltration rate of 1-inch per hour. Testing will be performed to confirm the design of the infiltration practices.

The infiltration practices are sized to treat at a minimum the peak WQv from the contributing areas, while allowing portions of larger storms to discharge from the infiltration practice through an overflow pipe or weir as allowed by the NYSSMDM. The overflow pipe and weir are set to allow the full WQv storage within the practices. The calculation of the WQv is performed per the methods of the NYSSMDM in Appendix A. Pretreatment has been provided for the proposed subsurface infiltration system in the form of a hydrodynamic separator. The peak flow for the 1-year storm was used to size the hydrodynamic separator used as pretreatment for the infiltration units. The data (including capacities) for the hydrodynamic separators are included in Appendix I. The table below summarizes the WQv-year peak flows and hydrodynamic separate flow rates.

Table 2.2.2 – Pretreatment	Hydrodynamic	Separator	Summary
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Subcatchment	WQv <sup>1</sup> Peak Flow (C.F.S).	Hydrodynamic Separator Model	Hydrodynamic Separator Capacity (C.F.S.)
1.2S	1.19	HydroStorm HS 5	1.37 CFS
1 = 1 + 11 +	1 1 1 1		

For detailed calculations see Appendix A

As noted in the table above the capacity of the hydrodynamic separator exceeds the calculated WQv peak flow. The hydrodynamic separator has an internal bypass capable of passing the flows from the contributing areas from the larger storm events.

Pretreatment for the proposed infiltration basin will be provided through a dry extended detention basin. The basin has been sized to provide greater than 24-hour extended detention of the center-of-mass of the 1-year, 24-hour storm event from the constributing area.

#### 2.3 NYSDEC Stream Channel Protection Volume, CPv

The Stream Channel Protection ( $CP_v$ ) criterion is intended to protect stream channels from erosion and is accomplished by the 24-hour extended detention of the one-year, 24-hour storm event. As shown in Appendix C, the proposed stormwater management systems have been designed to fully infiltrate the stormwater runoff from the 1-year, 24-hour design storm, therefore the CPv has been met for the proposed areas of new development. It should also be noted that the extended detention basin (1.1 EDB) has been designed to provide greater than 24-hour extended detention of the center-of-mass of the 1-year, 24-hour storm event, therefore also meeting the CRv requirement.

## 2.4 NYSDEC Overbank Flood Control, Qp, and Extreme Flood Control, Qf

The Overbank Flood Control ( $Q_p$ ) requirement is intended to prevent an increase in the frequency and magnitude of out-of-bank flooding events generated by urban development. Overbank control requires storage to attenuate the post-development 10-year, 24-hour peak discharge to predevelopment rates. The Extreme Flood Control ( $Q_f$ ) requirement is intended to prevent the increased risk of flood damage from large storm events, maintain the boundaries of the pre-development 100year flood plain, and protect the physical integrity of stormwater management practices. Extreme flood control requires storage to attenuate the post-development 100-year, 24-hour peak discharge to pre-development rates. As shown in Table 2.4.1 attenuation for both the 10-year and 100-year 24-hour storms has been provided thus satisfying the  $Q_p$  and  $Q_f$  requirements. The following table summarizes the pre and post development peak flows expected for the proposed project.

24-HOUR DESIGN STORM PEAK FLOWS (c.f.s.)							
	10-YEAR (Overbank Flood Control)PrePost		100-YEAR (Extreme Flood Control)				
			Pre	Post			
Design Line 1	43.1	43.0	93.6	92.0			

Table 2.4.1– Pre and Post-Development Peak Flows

As shown in the above table the peak flows discharging to the design line in the proposed condition have been mitigated to slightly below the existing condition levels. Since the rate of runoff in the proposed condition is less than the existing condition, the proposed onsite stormwater improvements will mitigate the potential impact of the peak flows downstream in the final condition.

## 3.0 STORMWATER CONVEYANCE SYSTEM

The stormwater collection and conveyance systems for the project will consist of catch basins, drain inlets, drainage manholes, swales and HDPE pipe. The system will be sized to collect and convey at minimum the 100-year, 1-hour design storm using the Rational Method. The Rational Method is a standard method used by engineers to develop flow rates for sizing collection systems. The Rational Method calculates flows based on a one-hour design storm. Calculations shall be provided in future reports.

#### 4.0 EROSION AND SEDIMENT CONTROL

Erosion and sediment control should be accomplished by four basic principles: diversion of clean water, containment of sediment, treatment of dirty water, and stabilization of disturbed areas. Diversion of clean water should be accomplished with swales. This diverted water should be safely conveyed around the construction area as necessary and discharged downstream of the disturbed areas. Sediment should be contained with the use of silt fence at the toe of disturbed slopes and excavation of the temporary sediment basin. Disturbed areas should be permanently stabilized within 14 days of final grading to limit the required length of time that the temporary facilities must be utilized. The owner will be responsible for the maintenance of the temporary erosion control facilities.

4.1 Temporary Erosion and Sediment Control Facilities

Temporary erosion and sediment control facilities should be installed and maintained as required to reduce the impacts to off-site properties. The owner will be required to provide maintenance for the temporary erosion and sediment control facilities. In general, the following temporary methods and materials should be used to control erosion and sedimentation from the project site:

- Stabilized Construction Entrance
- Silt Fence Barriers
- Storm Drain Inlet Protection

A stabilized construction entrance should be installed at the entrance to the site as shown on the plan. The design drawings will include details to guide the contractor in the construction of this entrance. The intent of the stabilized construction entrance is to prevent the "tracking" of soil from the site. Dust control should be accomplished with water sprinkling trucks if required. During dry periods, sprinkler trucks should wet all exposed earth surfaces as required to prevent the transport of air-borne particles to adjoining areas.

Siltation barriers constructed of geosynthetic filter cloth should be installed at the toe of all disturbed slopes. The intent of these barriers is to contain silt and sediment at the source and inhibit its transport by stormwater runoff. The siltation barriers will also help reduce the rate of runoff by creating filters through which the stormwater must pass.

#### 4.2 Permanent Erosion and Sediment Control Facilities

Permanent erosion and sediment control will be accomplished by diverting stormwater runoff from steep slopes, controlling/reducing stormwater runoff velocities and volumes, and vegetative and structural surface stabilization. All of the permanent facilities are relatively maintenance free and only require periodic inspections. The owner will provide maintenance for all the permanent erosion and sediment control facilities.

The temporary sediment trap shall be cleaned of all sediment and debris, and converted to an extended detention dry stormwater basin per the final elevations and dimensions, and stabilized with the vegetation as indicated on the project drawings. Riprap aprons will be used at the discharge end of all piped drainage systems. Runoff velocities will be reduced to levels that are non-erosive to the receiving waterbodies through use of these aprons.

Other than the buildings and paved surfaces, disturbed surfaces will be stabilized with vegetation. The vegetation will control stormwater runoff by preventing soil erosion, reducing runoff volume and velocities, and providing a filter medium. Permanent seeding should optimally be undertaken in the spring from March 21<sup>st</sup> through May 20<sup>th</sup> and in late summer from August 15<sup>th</sup> to October 15<sup>th</sup>.

#### 5.0 IMPLEMENTATION, MAINTENANCE & GENERAL HOUSEKEEPING

#### 5.1 Construction Phase

Details associated with the implementation and maintenance of the proposed stormwater facilities and erosion control measures during construction are shown on the project drawings. A Construction Sequence has been provided to guide the contractor in the installation of the erosion control measures as well as the site plan features. In accordance with NYSDEC SPDES General Permit GP-0-15-002 no phase will exceed the maximum of 5 acres of disturbance at any given time as less than 5 acres of disturbance is proposed. The erosion control plan includes associated details and notes to aid the contractor in implementing the plan.

During construction, a Site Log Book, Appendix E, is required to be kept per NYSDEC SPDES General Permit GP-0-15-002. Erosion and sediment control inspections are required to be conducted as necessary under coverage of the permit (minimum twice a week) and an updated logbook and a copy of the SWPPP is required to be kept on site for the duration of the construction activities. The Construction Site Log Book is an appendix taken from the *New York Standards and Specifications for Erosion and Sediment Control* (Blue Book).

In addition to the proposed erosion and sediment control facilities, the following good housekeeping best management practices shall be implemented to mitigate potential pollution during the construction phase of the project. The general contractor overseeing the day-to-day site operation shall be responsible for the good housekeeping best management practices included in the following general categories:

- Material Handling and Waste Management
- Establishment of Building Material Staging Areas
- Establishment of Washout Areas
- Proper Equipment Fueling and Maintenance Practices
- Spill Prevention and Control Plan

All construction waste materials shall be collected and removed from the site regularly by the general contractor. The general contractor shall supply waste barrels for proper disposal of waste materials. All personnel working on the site shall be instructed of the proper procedures for construction waste disposal.

Although it is not anticipated any hazardous waste materials will be utilized during construction, any hazardous waste materials shall be disposed of in accordance with federal, state, and local regulations. No hazardous waste shall be disposed of on-site. Hazardous waste materials shall be stored in appropriate and clearly marked containers and segregated from the other non-waste materials. All hazardous waste shall be stored in a structurally sound and sealed shipping containers located in the staging areas. Material safety data sheets, material inventory, and emergency contact numbers will be maintained in the office trailer. All personnel working on the site shall be instructed of the proper procedures for hazardous waste disposal.

Temporary sanitary facilities (portable toilets) shall be provided on site during the entire length of construction. The sanitary facilities shall be in an alternate area away from the construction activities on the site. The portable toilets shall be inspected weekly for evidence of leaking holding tanks.

All recyclables, including wood pallets, cardboard boxes, and all other recyclable construction scraps shall be disposed of in a designated recycling barrel provided by the contractor and removed from the site regularly. All personnel working on the site shall be instructed of the proper procedures for construction waste recycling.

All construction equipment and maintenance materials shall be stored in a designated staging area. Silt fence shall be installed down gradient of the construction staging area. Shipping containers shall be utilized to store hand tools, small parts, and other construction materials, not taken off site daily. Construction waste barrels, recycling barrels and if necessary hazardous waste containers shall be located within the limits of the construction staging area.

Throughout the construction of the project, several types of vehicles and equipment will be used onsite. Fueling of the equipment shall occur within the limits of the construction staging area. Fuel will be delivered to the site as needed, by the general contractor, or a party chosen by the general contractor. Only minor vehicle equipment maintenance shall occur on-site, all major maintenance shall be performed off-site. All equipment fluids generated from minor maintenance activities shall be disposed of into designated drums and stored in accordance with the hazardous waste storage as previously discussed.

Vehicles and equipment shall be inspected on each day of use. Any leak discovered shall be repaired immediately. All leaking equipment unable to be repaired shall be removed from the site. Ample supplies of absorbent, spill-cleanup materials, and spill kits shall be located in the construction staging area. All spills shall be cleaned up immediately upon discovery. Spent absorbent materials and rags shall be hauled off-site immediately after the spill is cleaned for disposal at a local landfill. All personnel working on the site shall be instructed of the proper procedures for spill prevention and control. Any spill large enough to discharge to surface water will be immediately reported to the local fire / police departments and the National Response Center 1-800-424-8802.

During the initial year of planting, the plants may require watering to germinate and establish. Note that several seedings may be required during the first year to completely establish vegetation on the site.

#### 5.2 Long Term Maintenance Plan

Each spring the paved areas should be cleaned to remove the winter's accumulation of traction sand. After this is completed, all drain inlets sumps and the stormwater basins should be cleaned. All pipes should be checked for debris and blockages and cleaned as required. During the cleaning process, the drain inlets, catch basins, and pipes should be inspected for structural integrity and overall condition; repairs and/or replacement will be made as required.

The stormwater facilities for the subject project have been designed to minimize the required maintenance. This section discusses the minimum maintenance requirements to insure long-term performance of the stormwater facilities. Initially the stormwater facilities will require an increased

maintenance and inspection schedule until all portions of the site are stable. Generally, the stormwater facilities consist of either collection and conveyance components or treatment components.

The stormwater collection and conveyance system is composed of HDPE, drainage pipe and precast concrete drainage structures. The owner will assume the maintenance responsibilities for the drainage system. Minimal maintenance is typically required for these facilities. All pipes should be checked for debris and blockages and cleaned as required. All drain inlet sumps, including the sumps within the hydrodynamic separators, shall be inspected bi-annually and cleaned to removed deposited sediment. During the cleaning process, the pipes should be inspected for structural integrity and overall condition; repairs and/or replacement should be made as required. Additionally, the detention systems shall be checked for deposited sediment as well. Visual inspection of system through the inspection ports shall take place yearly, and the system shall be cleaned / jetted as necessary to remove deposited sediment.

The stormwater facilities have been designed to limit the routine maintenance requirements. Initially the filter will require regular maintenance until the permanent vegetation is established. Permanent vegetation is considered established when 80% of the final plant density is established. Vegetation should be inspected weekly during construction as part of coverage under NYSDEC SPDES General Permit GP-0-15-002 during construction and in the permanent condition. Damaged areas should be immediately re-seeded and re-mulched. The floor of the filter will be planted with a seed mixture that contains plants that are tolerant of occasional flooding. The seed mixtures contain several plant species that vary slightly in their needs for survival. It is expected that not all of the species will survive within the basin due to variations such as water, nutrients, and light. During the initial year of planting, the plants may require watering to germinate and become established. Note that several seedings may be required during the first year to completely establish vegetation within the basin. After the initial year of establishment, the filter does not need to be fertilized or watered. A natural selection process will occur over the first few years, such that the species within the seed mixture most suitable to the conditions will survive.

Refer to the Infiltration Trench and Basin Inspection & Maintenance checklist found in Appendix G of this report prepared for all portions of this project the requirements to insure long-term performance of all stormwater facilities

Refer to the Hydroworks Hydrostorm Operations & Maintenance Manual in Appendix H of this report for the manufacture maintenance requirements for the proposed hydrodynamic separator.

# **APPENDIX A**

NYSDEC Water Quality Volume and Runoff Reduction Calculations

## **WQv Calculation Worksheet**

1.1

Project:Beacon Views, LLCProject #:19131.100Date:8/16/2019



The following calculation determines the water quality flow rate for the 90% Water Quality Event using the Small Storm Hydrology Method specified in Appendix B of the New York State Stormwater Management Design Manual.

#### Subcatchment ID:

1 Water Quality Volume – $WQ = \frac{P * R_v * A}{V}$			
$\frac{12}{12}$			
P = WQv 24-hour Rainfall Amount	=	1.4 in.	
A = Subcatchment Area	=	141250 SF	
Ai= Impervious Area within Subcatchment Area	=	82800	
I = Ai/A	=	58.6 %	
Rv = 0.05 + 0.009 (1%)	=	0.58	
WQv = Water Quality Volume	=	9,558 CF	

Subcatchment ID:	1.2		
1.Water Quality Volume $= W($	$Q_{\nu} = \frac{P * R_{\nu} * A}{12}$		
	P = WQv 24-hour Rainfall Amount	=	1.4 in.
	A = Subcatchment Area	=	21160 SF
	Ai= Impervious Area within Subcatchment Area	=	13350
	I = Ai/A	=	63.1 %
	Rv = 0.05 + 0.009 (I%)	=	0.62
	WQv = Water Quality Volume	=	1,531 CF

#### **RRv Calculation Worksheet - Infiltration Basin 1.1 INF** Project: Beacon Views, LLC



Project #: 19131.100		ENG LAND	ineering, s SCAPE ARCHIT	URVEYING & TECTURE, P.C.
1 RRv Initial = Water	r Quality Volume (WQv)	0.219 ac-ft		9.558 c.f
(refer to Water Qualit	v Volume Calculation Sheet)	0.210 40 1	_	0,000 0
	y volume outoutation enocity			
2 BBy Minimum =	[(P)(By)(S)(Aic)]/12 where			
	P = Bainfall (in.)		=	1.40 in
	Bv = 0.05 + 0.009(59%)		=	0.59
	S = Hydrologic Soil Group Specific Reduction	Factor	=	0.20
	HSG A = 0.551 HSG B = 0.401 HSG C =	0.301 [HSG D = 0.20]		0.20
	Aic = Total area of new impervious cover		=	1.9 Acres
	RRv Minimum		=	1,140 c.f.
3. RRv Required = R	Rv Initial - Green Infrastructure Practice (GIP)	with Area Reduction		
GIP with A	Area Reduction Applied in Project			
5.3.1 Con	servation of Natural Area		N/A	Ą
5.3.2 She	et Flow to Riparian Buffers or Filter Strips		N/A	4
5.3.4 Tree	e Planting / Tree Box (37 trees at 100 s.f. pe	er tree)		c.f.
5.3.5 Disc	connection of Rooftop Runoff			-
5.3.6 Stre	am Daylighting		N/A	A
RRv Requ	uired(=WQv-RRV by area)(Refer to HydroCAD	output in this Appendix)	=	9,558 c.f.

4. RRv Provided			
GIP with Volume Reduction Applied in Project	WQv Treated (c.f.)	% of WQv Applied to <i>RRv</i> <i>Provided</i>	RRv Provided (c.f.)
5.3.3 Vegetated Open Swales		20%	0
[HSG A / B = 20%] [HSG C / D = 10%] {Modified HSG C - D = 15% - 12%]		10%	0
5.3.7 Rain Garden		40%	0
[No underdrains / Good Soils = 100%] [With underdrains / Poor Soils = 40%]			
5.3.8 Green Roof		100%	N/A
[RRv provided equals volume provided in Green Roof]			
5.3.9 Stormwater Planters		45%	N/A
[Infiltration Planters = 100%] [Flow Through HSG C = 45%] [Flow Though HSG D = 30%]			
5.3.10 Rain Tank / Cisterns		100%	N/A
5.3.11 Porous Pavement		100%	0
Infiltration Practice (Standard SMP)	9650	100%	9,650
Bioretention Practice (Standard SMP)		40%	0
[Without Underdrains HSG A/B = 80%] [With Underdrain HSG C\D = 40%]			
Dry Swale (Open Channel Practice) (Standard SMP)		20%	N/A
[HSG A/B = 40%] [HSG C/D = 20%]			
RRv Provided =			9,650

5. Summary

RRv Initial	=	9,558 c.f.	
RRv Required	=	9,558 c.f.	
RRv Minimum	=	1,140 c.f.	
RRv Provided	=	9,650 c.f.	
WQv Required for Downstream SMP	=	0 c.f.	(= RRv Required - RRv Provided)
Is RRv Provided greater than or equal to RRv Minimum?		Yes	

Refer to the "Analysis of Green Infrastructure Practices" contained in Appendix F for an explanation demonstrating the maximum RRv Provided has been achieved for the site.

## **RRv Calculation Worksheet - Infiltration System 1.2 INF**

N S | T E Beacon Views, LLC Project: ENGINEERING, SURVEYING & Project #: 19131.100 LANDSCAPE ARCHITECTURE, P.C. Date: 8/20/2019 1. RRv Initial = Water Quality Volume (WQv) 0.035 ac-ft 1.531 c.f. = (refer to Water Quality Volume Calculation Sheet) [(P)(Rv)(S)(Aic)]/12 2. RRv Minimum = where... P = Rainfall (in.)1.40 in. = Rv = 0.05 + 0.009 (63%)0.62 = S = Hydrologic Soil Group Specific Reduction Factor 0.20 = [HSG A = 0.55] [HSG B = 0.40] [HSG C = 0.30] [HSG D = 0.20] Aic = Total area of new impervious cover 0.3 Acres RRv Minimum 193 c.f. 3. RRv Required = RRv Initial - Green Infrastructure Practice (GIP) with Area Reduction GIP with Area Reduction Applied in Project 5.3.1 Conservation of Natural Area N/A 5.3.2 Sheet Flow to Riparian Buffers or Filter Strips N/A 5.3.4 Tree Planting / Tree Box (37 trees at 100 s.f. per tree) c.f. 5.3.5 Disconnection of Rooftop Runoff 5.3.6 Stream Daylighting N/A RRv Required(=WQv-RRV by area)(Refer to HydroCAD output in this Appendix) 1,531 c.f. =

4. RRv Provided % of WQv WQv RRv Applied to GIP with Volume Reduction Applied in Project Treated Provided RRv (c.f.) (c.f.) Provided 5.3.3 Vegetated Open Swales 20% 0 10% [HSG A / B = 20%] [HSG C / D = 10%] {Modified HSG C - D = 15% - 12%] 0 5.3.7 Rain Garden 40% 0 [No underdrains / Good Soils = 100%] [With underdrains / Poor Soils = 40%] 100% N/A 5.3.8 Green Roof [RRv provided equals volume provided in Green Roof] 5.3.9 Stormwater Planters 45% N/A [Infiltration Planters = 100%] [Flow Through HSG C = 45%] [Flow Though HSG D = 30%] 5.3.10 Rain Tank / Cisterns 100% N/A 5.3.11 Porous Pavement 100% 0 Infiltration Practice (Standard SMP) 1917 100% 1,917 Bioretention Practice (Standard SMP) 40% 0 [Without Underdrains HSG A/B = 80%] [With Underdrain HSG C\D = 40%] Dry Swale (Open Channel Practice) (Standard SMP) 20% N/A [HSG A/B = 40%] [HSG C/D = 20%] RRv Provided = 1,917

5. Summary

Is RRv

RRv Initial	=	1,531 c.f.	
RRv Required	=	1,531 c.f.	
RRv Minimum	=	193 c.f.	
RRv Provided	=	1,917 c.f.	
WQv Required for Downstream SMP	=	0 c.f.	(= RRv Required - RRv Provided)
Provided greater than or equal to RRv Minimum?		Yes	

Refer to the "Analysis of Green Infrastructure Practices" contained in Appendix F for an explanation demonstrating the maximum RRv Provided has been achieved for the site.

# **APPENDIX B**

Pre-Development Computer Data



Pre Development	NY-Beacon 24-hr S0P 1-yr	Rainfall=2.61"
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# Summary for Subcatchment PRE:

Runoff = 14.68 cfs @ 12.37 hrs, Volume= 1.558 af, Depth> 0.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 1-yr Rainfall=2.61"

Area (	ac) C	N Dese	cription		
8.9	900 7	78 Mea	dow, non-g	grazed, HS	G D
17.2	200 7	77 Woo	ds, Good,	HSG D	
0.2	200 9	8 Pave	ed parking	, HSG D	
26.3	300 7	7 Weig	ghted Aver	age	
26.1	100	99.2	4% Pervio	us Area	
0.2	200	0.76	% Impervi	ous Area	
_					
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
13.9	100	0.0600	0.12		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.16"
4.7	345	0.0600	1.22		Shallow Concentrated Flow,
			4.00		Woodland Kv= 5.0 fps
1.4	1/0	0.0800	1.98		Shallow Concentrated Flow,
0.0	0.40	0 1 0 0 0	1 50		Short Grass Pasture Kv= 7.0 fps
3.6	340	0.1000	1.58		Shallow Concentrated Flow,
ΕO	400	0 0700	1 00		woodland KV= 5.0 lps
5.0	400	0.0700	1.32		Woodland Ky 5.0 fre
	4 055	<b>T</b> . I . I			$\frac{1}{1000}$
28.6	1,355	iotai			

## **Pre Development**



## Subcatchment PRE:

Pre Development	NY-Beacon 24-hr S0P	10-yr Rainfall=4.70"
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# Summary for Subcatchment PRE:

Runoff = 43.11 cfs @ 12.36 hrs, Volume= 4.716 af, Depth> 2.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 10-yr Rainfall=4.70"

Area (	(ac) C	N Des	cription		
8.9	900 7	78 Mea	dow, non-g	grazed, HS	G D
17.2	200 7	77 Woo	ods, Good,	HSG D	
0.2	200 9	8 Pave	ed parking	, HSG D	
26.3	300 7	7 Weig	ghted Aver	age	
26.1	100	99.2	4% Pervio	us Area	
0.2	200	0.76	% Impervi	ous Area	
_					
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
13.9	100	0.0600	0.12		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.16"
4.7	345	0.0600	1.22		Shallow Concentrated Flow,
			4		Woodland Kv= 5.0 fps
1.4	170	0.0800	1.98		Shallow Concentrated Flow,
0.0	0.40	0 1 0 0 0	1 50		Short Grass Pasture Kv= 7.0 tps
3.6	340	0.1000	1.58		Shallow Concentrated Flow,
ΕO	400	0 0700	1 00		woodland KV= 5.0 lps
5.0	400	0.0700	1.32		Shallow Concentrated Flow, Woodland Ky 5.0 fpc
	1 055	Tatal			$\frac{1}{1000}$
28.6	1,355	rotal			

# **Pre Development**

Hydrograph 48-46-- Runoff 43.11 cfs 44 42 NY-Beacon 24-hr S0P 10-yr 40-38-Rainfall=4.70" 36-34-Runoff Area=26.300 ac 32 Runoff Volume=4.716 af 30-28 Flow (cfs) Runoff Depth>2.15" 26 24 22 Flow Length=1,355' 20 Tc=28.6 min 18 16 CN=77 14-12-10-8-6-4-2-0-6 ż 8 ģ 11 12 14 15 16 17 18 19 5 10 13 20 Time (hours)

## Subcatchment PRE:

Pre Development	NY-Beacon 24-hr S0P	100-yr Rainfall=8.31"
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# Summary for Subcatchment PRE:

Runoff = 93.60 cfs @ 12.35 hrs, Volume= 11.266 af, Depth> 5.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 100-yr Rainfall=8.31"

Area	(ac) C	N Des	cription					
8.	900	78 Mea	Meadow, non-grazed, HSG D					
17.	200	77 Woo	ods, Good,	HSG D				
0.	200	98 Pav	ed parking	, HSG D				
26.300 77 V			Weighted Average					
26.	100	99.2	4% Pervio	us Area				
0.200		0.76	% Impervi	ous Area				
_				_				
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
13.9	100	0.0600	0.12		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 3.16"			
4.7	345	0.0600	1.22		Shallow Concentrated Flow,			
	470		4 00		Woodland Kv= 5.0 fps			
1.4	170	0.0800	1.98		Shallow Concentrated Flow,			
0.0	040	0 1000	1 50		Short Grass Pasture KV= 7.0 tps			
3.0	340	0.1000	1.58		Shallow Concentrated Flow,			
5.0	400	0 0700	1 00		Shallow Concentrated Flow			
5.0	400	0.0700	1.52		Woodland Ky= 5.0 fps			
00.0	1 055	Total						
28.6	ା,୪୦୦	rotai						

# **Pre Development**



# Subcatchment PRE:

# **APPENDIX C**

Post-Development Computer Data



Post Development	NY-Beacon 24-hr S0P 1-y	r Rainfall=2.61"
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# Summary for Subcatchment 1.0S:

Runoff = 13.57 cfs @ 12.37 hrs, Volume= 1.613 af, Depth= 0.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 1-yr Rainfall=2.61"

_	Area	(ac) C	N Dese	cription			
8.900 78 Meadow, non-grazed, HSG D						G D	
	13.	400 7	77 Woo	ds, Good,	HSG D		
	0.	200 9	98 Pave	ed parking	, HSG D		
22.500 78 Weighted Average							
22.300 99.11% Pervious Area							
	0.200 0.89% Impervious Area				ous Area		
				•			
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	13.9	100	0.0600	0.12		Sheet Flow,	
						Woods: Light underbrush n= 0.400 P2= 3.16"	
	4.7	345	0.0600	1.22		Shallow Concentrated Flow,	
						Woodland Kv= 5.0 fps	
	1.4	170	0.0800	1.98		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	3.1	280	0.0900	1.50		Shallow Concentrated Flow,	
						Woodland Kv= 5.0 fps	
	0.5	225		7.50		Direct Entry, Channel Flow	
	0.0	36				Direct Entry, Pipe Flow	
	0.5	360		12.00		Direct Entry, Channel Flow	
	4.3	30	0.1000	0.12		Sheet Flow,	
_						Woods: Light underbrush n= 0.400 P2= 3.16"	

28.4 1,546 Total

# Post DevelopmentNY-Beacon 24-hr SOP 1-yrRainfall=2.61"Prepared by Insite Engineering, Surveying & Landscape Architecture, P.C.Printed 8/27/2019HydroCAD® 10.00-15 s/n 02171 © 2015 HydroCAD Software Solutions LLCPage 3

Subcatchment 1.0S:


Post Development	NY-Beacon 24-hr S0P 1-yr Rail	nfall=2.61"
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## Summary for Subcatchment 1.1S:

Runoff = 7.82 cfs @ 12.03 hrs, Volume= 0.448 af, Depth= 1.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 1-yr Rainfall=2.61"

Ar	ea	(ac) CN	Des	cription		
	1.	900 98	B Pave	ed parking	, HSG D	
	1. 3. 1. 1.	400 80 300 90 400 900	0 >75 0 Weig 42.4 57.5	ghted Ave 2% Pervic 8% Impervic	rage pus Area vious Area	I, IISG D
- (mi	Tc n)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5	.0					Direct Entry,
					Subca	atchment 1.1S:
					Hydro	ograph
	- - 8 -		7.82 cfs			
	7-		     · -  - ·		               - + - + - + - + -	NY-Beacon 24-hr S0P 1-yr
	-					Rainfall=2.61"
	6					Runoff Volume=0.448 af
w (cfs)	-					Runoff Depth=1.63"
Flo	4		· -¦¦- ·			Tc=5.0 min
	3		· -¦¦- ·			- + - + - + - + - + - + - + - + - + - +
	2					
	1-	$-\frac{1}{1}$ $-\frac{1}{1}$ $-\frac{1}{1}$ $-\frac{1}{1}$ $-\frac{1}{1}$	· -¦   -¦- ·	$-\frac{1}{1}\frac{1}{1}\frac{1}{1}\frac{1}{1}\frac{1}{1}\frac{1}{1}$	$\frac{1}{1} - \frac{1}{1} - \frac{1}$	
	0	· · · · ·				
	0	2468	10 12 14	16 18 20 22 2	4 26 28 30 32 Tii	34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 ime (hours)

Post Development	NY-Beacon 24-hr S0P 1-yr Ra	infall=2.61"
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#### Summary for Subcatchment 1.2S:

Runoff = 1.24 cfs @ 12.03 hrs, Volume= 0.071 af, Depth= 1.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 1-yr Rainfall=2.61"



Post Development	NY-Beacon 24-hr S0P 1-y	r Rainfall=2.61"
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## Summary for Reach Design Line:

Inflow A	Area :	=	26.300 ac,	9.16% Imperviou	s, Inflow Depth	= 0.7	<sup>7</sup> 4" for 1-y	r event
Inflow	=	=	13.57 cfs @	12.37 hrs, Volur	ne= 1.6 <sup>-</sup>	13 af		
Outflow	/ =	=	13.57 cfs @	12.37 hrs, Volur	ne= 1.6 <sup>-</sup>	13 af,	Atten= 0%,	Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

#### **Reach Design Line:**



#### Summary for Pond 1.1 EDB:

Inflow Area =	3.300 ac, 57.58%	Impervious, Inflow Depth =	1.63" for 1-yr event
Inflow =	7.82 cfs @ 12.03	hrs, Volume= 0.44	8 af
Outflow =	0.10 cfs @ 21.85	hrs, Volume= 0.44	7 af, Atten= 99%, Lag= 588.9 min
Primary =	0.10 cfs @ 21.85	hrs, Volume= 0.44	7 af
Secondary =	0.00 cfs @ 0.00	hrs, Volume= 0.00	0 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 185.21' @ 21.85 hrs Surf.Area= 7,934 sf Storage= 14,267 cf

Plug-Flow detention time= 1,441.5 min calculated for 0.447 af (100% of inflow) Center-of-Mass det. time= 1,440.8 min (2,262.8 - 822.0)

Volume	Invert	Avail.Stor	rage Storage D	escription			
#1	183.00'	30,70	00 cf Custom S	tage Data (Pri	smatic) Listed below (Recalc)		
Elevation (feet)	Su	ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
183.00 184.00 186.00 187.00		5,000 6,300 9,000 10,500	0 5,650 15,300 9,750	0 5,650 20,950 30,700			
Device R	outing	Invert	Outlet Devices				
#1 P	rimary	182.00'	<b>4.0'' Round Cu</b> L= 40.0' CPP, Inlet / Outlet Inv n= 0.013 Corru	I <b>lvert</b> square edge h vert= 182.00' / gated PE, smo	neadwall, Ke= 0.500 181.50' S= 0.0125 '/' Cc= 0.900 poth interior, Flow Area= 0.09 sf		
#2 D #3 S	evice 1 econdary	182.00' 183.00'	<b>1.5'' Vert. Orifice/Grate</b> $C=0.600$ <b>24.0'' Round Culvert</b> L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 183.00' / 182.00' S= 0.0200 '/' Cc= 0.900				
#4 D	evice 3	185.50'	8.0' long x 0.5' Head (feet) 0.2 Coef. (English)	breadth Broa 0 0.40 0.60 2.80 2.92 3.0	d-Crested Rectangular Weir 0.80 1.00 08 3.30 3.32		
Primary OutFlow Max=0.10 cfs @ 21.85 hrs HW=185.21' (Free Discharge) 1=Culvert (Passes 0.10 cfs of 0.49 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.10 cfs @ 8.54 fps)							

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=183.00' (Free Discharge) -3=Culvert (Controls 0.00 cfs) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

## Post DevelopmentNY-Beacon 24-hr SOP 1-yrRainfall=2.61"Prepared by Insite Engineering, Surveying & Landscape Architecture, P.C.Printed 8/27/2019HydroCAD® 10.00-15 s/n 02171 © 2015 HydroCAD Software Solutions LLCPage 8

Pond 1.1 EDB:



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Elevation	Surface	Storage	Elevation	Surface	Storage
	(SQ-II)			(sq-ii)	
183.00	5,000	0	185.60	8,460	17,458
183.05	5,065	252	185.65	8,528	17,883
183.10	5,130	506	185.70	8,595	18,311
183.15	5,195	765	185.75	8,663	18,742
183.20	5,260	1,026	185.80	8,730	19,177
183.25	5,325	1,291	185.85	8,797	19,615
183.30	5,390	1,559	185.90	8,865	20,057
183.35	5,455	1,830	185.95	8,932	20,502
183.40	5,520	2,104	186.00	9,000	20,950
183.45	5,585	2,382	186.05	9,075	21,402
183.50	5,650	2,663	186.10	9,150	21,857
183.55	5,715	2,947	186.15	9,225	22,317
183.60	5,780	3,234	186.20	9,300	22,780
183.65	5,845	3,525	186.25	9,375	23,247
183.70	5,910	3,818	186.30	9,450	23,/18
183.75	5,975	4,116	186.35	9,525	24,192
183.80	6,040	4,416	186.40	9,600	24,670
183.85	6,105	4,720	186.45	9,675	25,152
183.90	6,170	5,027	186.50	9,750	25,638
183.95	6,235	5,337	186.00	9,825	26,127
184.00	6,300	5,65U	186.60	9,900	20,020
184.05	0,308	5,967	180.00	9,975	27,117
184.10	6,435	6,287 6,610	186.70	10,050	27,017
104.10	6,503	6,010	100.75	10,120	20,122
104.20	6,570	0,937	196.00	10,200	20,030
184.20	6 705	7,207	186.00	10,275	29,142
104.30	6 772	7,001	196.90	10,350	29,000
184.33	6.840	8 278	187.00	10,423	<b>30</b> ,177
184.40	6 907	8 622	107.00	10,500	30,700
184.50	6 975	8 969			
184 55	7 0/3	0,303			
184 60	7,040	9 673			
184.65	7,178	10,030			
184 70	7 245	10,000			
184 75	7,240	10,001			
184 80	7,380	11 122			
184.85	7,447	11,493			
184.90	7.515	11.867			
184.95	7.582	12.244			
185.00	7.650	12.625			
185.05	7.718	13.009			
185.10	7,785	13,397			
185.15	7,853	13,788			
185.20	7,920	14,182			
185.25	7,988	14,580			
185.30	8,055	14,981			
185.35	8,122	15,385			
185.40	8,190	15,793			
185.45	8,257	16,204			
185.50	8,325	16,619			
185.55	8,393	17,037			

#### Stage-Area-Storage for Pond 1.1 EDB:

Post Development	NY-Beacon 24-hr S0P 1-	yr Rainfall=2.61"
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#### Summary for Pond 1.1 INF:

Inflow Area	ι =	3.300 ac, 5	7.58% Imp	ervious,	Inflow De	epth >	1.62	2" for	1-yr	event	
Inflow	=	0.10 cfs @	21.85 hrs,	Volume	=	0.447	af				
Outflow	=	0.09 cfs @	37.70 hrs,	Volume	=	0.446	af, /	Atten=	11%,	Lag= 9	50.9 min
Discarded	=	0.09 cfs @	37.70 hrs,	Volume	=	0.446	af				
Primary	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af				

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 180.26' @ 37.70 hrs Surf.Area= 4,029 sf Storage= 1,011 cf

Plug-Flow detention time= 109.5 min calculated for 0.446 af (100% of inflow) Center-of-Mass det. time= 106.2 min (2,369.0 - 2,262.8)

Volume	Invert	Avail.Stor	age Storage	Description		
#1	180.00'	16,15	i0 cf Custom	n Stage Data (Pri	ismatic) Listed below (Recalc)	
Elevatio (fee 180.0 182.0 183.0	on Su et) 00 00 00	urf.Area (sq-ft) 3,750 5,900 7,100	Inc.Store (cubic-feet) 0 9,650 6,500	Cum.Store (cubic-feet) 0 9,650 16,150		
Device	Routing	Invert	Outlet Device	es		
#1	Discarded	180.00'	1.000 in/hr E	xfiltration over H	Horizontal area	
#2	#2 Primary 182.00' <b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32					
Discard	ed OutFlow	Max=0.09 cfs	s @ 37.70 hrs	HW=180.26' (F	Free Discharge)	

**1=Exfiltration** (Exfiltration Controls 0.09 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=180.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

## Post DevelopmentNY-Beacon 24-hr S0P 1-yr Rainfall=2.61"Prepared by Insite Engineering, Surveying & Landscape Architecture, P.C.Printed 8/27/2019HydroCAD® 10.00-15 s/n 02171 © 2015 HydroCAD Software Solutions LLCPage 11

Pond 1.1 INF:



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#### Stage-Area-Storage for Pond 1.1 INF:

Elevation	Surface	Horizontal	Storage
(feet)	(sq-ft)	(sq-ft)	(cubic-teet)
180.00	3,750	3,750	0
180.10	3,857	3,857	380
180.20	3,965	3,965	771
180.30	4,073	4,073	1,173
180.40	4,180	4,180	1,586
180.50	4,288	4,288	2,009
180.60	4,395	4,395	2,443
180.70	4,502	4,502	2,888
180.80	4,610	4,610	3,344
180.90	4,718	4,718	3,810
181.00	4,825	4,825	4,288
181.10	4,932	4,932	4,775
181.20	5,040	5,040	5,274
181.30	5,148	5,148	5,783
181.40	5,255	5,255	6,304
181.50	5,363	5,363	6,834
181.60	5,470	5,470	7,376
181.70	5,577	5,577	7,928
181.80	5,685	5,685	8,492
181.90	5,793	5,793	9,065
182.00	5,900	5,900	9,650
182.10	6,020	6,020	10,246
182.20	6,140	6,140	10,854
182.30	6,260	6,260	11,474
182.40	6,380	6,380	12,106
182.50	6,500	6,500	12,750
182.60	6,620	6,620	13,406
182.70	6,740	6,740	14,074
182.80	6,860	6,860	14,754
182.90	6,980	6,980	15,446
183.00	7,100	7,100	16,150

Post Development	NY-Beacon 24-hr S0P 1-	yr Rainfall=2.61"
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#### Summary for Pond 1.2 FS:

Inflow Area =	0.500 ac, 6	62.00% Impervious,	Inflow Depth = 1.71"	' for 1-yr event
Inflow =	1.24 cfs @	12.03 hrs, Volume	= 0.071 af	
Outflow =	1.24 cfs @	12.03 hrs, Volume	= 0.071 af, At	tten= 0%, Lag= 0.0 min
Primary =	1.24 cfs @	12.03 hrs, Volume	= 0.071 af	-
Secondary =	0.00 cfs @	0.00 hrs, Volume	= 0.000 af	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 187.27' @ 12.03 hrs Flood Elev= 189.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	186.40'	<b>8.0'' Round Culvert</b> L= 20.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 186.40' / 185.80' S= 0.0300 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Secondary	186.40'	<b>12.0" Round Culvert</b> L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 186.40' / 185.50' S= 0.0180 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#3	Device 2	187.30'	<b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

**Primary OutFlow** Max=1.20 cfs @ 12.03 hrs HW=187.24' (Free Discharge) **1=Culvert** (Inlet Controls 1.20 cfs @ 3.43 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=186.40' (Free Discharge) 2=Culvert (Controls 0.00 cfs) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 1.2 FS:



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Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
186.40	Ó	187.44	0	188.48	0
186.42	0	187.46	0	188.50	0
186.44	0	187.48	0	188.52	0
186.46	0	187.50	0	188.54	0
186.48	0	187.52	0	188.56	0
186.50	0	187.54	0	188.58	0
186.52	0	187.56	0	188.60	0
186.54	0	187.58	0	188.62	0
100.00	0	187.60	0	100.04	0
186.60	0	107.02	0	188.68	0
186.62	0	187.66	0	188 70	0
186.64	0	187.68	0	188.72	0
186.66	0	187.70	0 0	188.74	0
186.68	0	187.72	0	188.76	0
186.70	0	187.74	0	188.78	0
186.72	0	187.76	0	188.80	0
186.74	0	187.78	0	188.82	0
186.76	0	187.80	0	188.84	0
186.78	0	187.82	0	188.86	0
186.80	0	187.84	0	188.88	0
186.82	0	187.86	0	188.90	0
180.84	0	187.88	0	188.92	0
186.88	0	107.90	0	188.96	0
186.90	0	187.92	0	188.98	0
186.92	0	187.96	0	189.00	0
186.94	ů 0	187.98	0 0		Ŭ
186.96	0	188.00	0		
186.98	0	188.02	0		
187.00	0	188.04	0		
187.02	0	188.06	0		
187.04	0	188.08	0		
187.06	0	188.10	0		
187.08	0	188.12	0		
107.10	0	100.14	0		
187.12	0	188 18	0		
187 16	0	188.20	0		
187.18	0	188.22	0		
187.20	0	188.24	0 0		
187.22	0	188.26	0		
187.24	0	188.28	0		
187.26	0	188.30	0		
187.28	0	188.32	0		
187.30	0	188.34	0		
187.32	0	188.36	0		
107.34	U	108.38	0		
107.30	0	188 /2	0		
187 40	0	188 44	0		
187.42	0	188.46	0		
	č		Ŭ		

#### Stage-Area-Storage for Pond 1.2 FS:

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#### Summary for Pond 1.2 INF:

Inflow Area	ι =	0.500 ac, 6	2.00% Impe	ervious,	Inflow Dept	h= 1	.71"	for 1-yr	event
Inflow	=	1.24 cfs @	12.03 hrs,	Volume	= 0.	071 a	f		
Outflow	=	0.03 cfs @	10.40 hrs,	Volume	= 0.	071 a	f, Attei	n= 98%,	Lag= 0.0 min
Discarded	=	0.03 cfs @	10.40 hrs,	Volume	= 0.	071 a	f		-
Primary	=	0.00 cfs @	0.00 hrs,	Volume	= 0.	000 at	f		

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 185.66' @ 16.49 hrs Surf.Area= 0.028 ac Storage= 0.041 af

Plug-Flow detention time= 625.6 min calculated for 0.071 af (100% of inflow) Center-of-Mass det. time= 625.5 min (1,442.3 - 816.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	183.50'	0.026 af	39.50'W x 30.92'L x 3.50'H Field A
			0.098 af Overall - 0.034 af Embedded = 0.064 af x 40.0% Voids
#2A	184.00'	0.034 af	ADS_StormTech SC-740 x 32 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 8 rows
		0.060 of	Total Available Storage

0.060 af Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	183.50'	1.000 in/hr Exfiltration over Horizontal area
#2	Primary	185.80'	8.0" Round Culvert
			L= 10.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 185.80' / 185.50' S= 0.0300 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf

**Discarded OutFlow** Max=0.03 cfs @ 10.40 hrs HW=183.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=183.50' (Free Discharge) -2=Culvert (Controls 0.00 cfs)

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Pond 1.2 INF:



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Elevation	Horizontal	Storage	Elevation	Horizontal	Storage
(feet)	(acres)	(acre-feet)	(feet)	(acres)	(acre-feet)
183.50	0.028	0.000	186.10	0.028	0.049
183.55	0.028	0.001	186.15	0.028	0.050
183.60	0.028	0.001	186.20	0.028	0.050
183.65	0.028	0.002	186.25	0.028	0.051
183.70	0.028	0.002	186.30	0.028	0.052
183.75	0.028	0.003	186.35	0.028	0.052
183.80	0.028	0.003	186.40	0.028	0.053
183.85	0.028	0.004	186.45	0.028	0.054
183.90	0.028	0.004	186.50	0.028	0.054
183.95	0.028	0.005	186.00	0.028	0.055
184.00	0.028	0.000	186.65	0.028	0.055
184 10	0.020	0.007	186 70	0.020	0.050
184 15	0.028	0.000	186 75	0.020	0.000
184.20	0.028	0.010	186.80	0.028	0.058
184.25	0.028	0.011	186.85	0.028	0.058
184.30	0.028	0.012	186.90	0.028	0.059
184.35	0.028	0.014	186.95	0.028	0.059
184.40	0.028	0.015	187.00	0.028	0.060
184.45	0.028	0.016			
184.50	0.028	0.017			
184.55	0.028	0.018			
184.60	0.028	0.019			
184.65	0.028	0.020			
184.70	0.028	0.021			
184.75	0.028	0.023			
104.00	0.028	0.024			
184.00	0.020	0.025			
184.95	0.020	0.020			
185.00	0.028	0.028			
185.05	0.028	0.029			
185.10	0.028	0.030			
185.15	0.028	0.031			
185.20	0.028	0.032			
185.25	0.028	0.033			
185.30	0.028	0.034			
185.35	0.028	0.035			
185.40	0.028	0.036			
185.45	0.028	0.037			
185.50	0.028	0.038			
100.00	0.028	0.039			
185.65	0.020	0.040			
185 70	0.020	0.041			
185.75	0.028	0.043			
185.80	0.028	0.044			
185.85	0.028	0.045			
185.90	0.028	0.046			
185.95	0.028	0.046			
186.00	0.028	0.047			
186.05	0.028	0.048			

#### Stage-Area-Storage for Pond 1.2 INF:

Post Development	NY-Beacon 24-hr S0P 1	0-yr Rainfall=4.70"
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## Summary for Subcatchment 1.0S:

Runoff = 38.40 cfs @ 12.35 hrs, Volume= 4.611 af, Depth= 2.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 10-yr Rainfall=4.70"

_	Area	(ac) C	N Dese	cription					
	8.900 78 Meadow, non-grazed, HSG D								
	13.	400	77 Woo	ods, Good,	HSG D				
	0.	200 9	98 Pave	ed parking	, HSG D				
	22.500 78 Weighted Average								
	22.300 99.11% Pervious Area								
	0.200 0.89% Impervious Area								
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	13.9	100	0.0600	0.12		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 3.16"			
	4.7	345	0.0600	1.22		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	1.4	170	0.0800	1.98		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	3.1	280	0.0900	1.50		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	0.5	225		7.50		Direct Entry, Channel Flow			
	0.0	36				Direct Entry, Pipe Flow			
	0.5	360		12.00		Direct Entry, Channel Flow			
	4.3	30	0.1000	0.12		Sheet Flow,			
_						Woods: Light underbrush n= 0.400 P2= 3.16"			
			<b>—</b>						

28.4 1,546 Total

Post Development	NY-Beacon 24-hr S0P	10-yr Rainfall=4.70"
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Subcatchment 1.0S:



Post Development	NY-Beacon 24-hr S0P 10-yr	Rainfall=4.70"
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## Summary for Subcatchment 1.1S:

Runoff = 14.74 cfs @ 12.03 hrs, Volume= 0.987 af, Depth= 3.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 10-yr Rainfall=4.70"

Area (ac) CN Description						
1.900 98 Paved parking, HSG D	L HSG D					
1.400     80     >75% Grass cover, Good, HSG D       3.300     90     Weighted Average       1.400     42.42% Pervious Area       1.900     57.58% Impervious Area						
Tc Length Slope Velocity Capacity (min) (feet) (ft/ft) (ft/sec) (cfs)	Description					
5.0	Direct Entry,					
Subca	atchment 1.1S:					
Hydro	ograph					
16 15 14 15 14 13 12 12 10 10 10 10 10 10 10 10 10 10	NY-Beacon 24-hr S0P 10-yr     Rainfall=4.70''     Runoff Area=3.300 ac     Runoff Volume=0.987 af     Runoff Depth=3.59''     Tc=5.0 min     CN=90					
2 1 1 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 2 2 2 2 2 2 2 2 2 2 2 2 2	1   1					
Ti	me (nours)					

Post Development	NY-Beacon 24-hr SOP 10-y	r Rainfall=4.70"
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## Summary for Subcatchment 1.2S:

Runoff = 2.28 cfs @ 12.03 hrs, Volume= 0.154 af, Depth= 3.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 10-yr Rainfall=4.70"

Area (ac	;) CN	Desc	ription			
0.310	0 98	Pave	d parking	, HSG D		
0.190	0 80	>75%	6 Grass co	over, Good,	, HSG D	
0.500	0 91	Weig	hted Aver	age		
0.190	0	38.00	0% Pervio	us Area		
0.310	0	62.00	0% Imperv	vious Area		
<b>-</b> .				<b>o</b> ''		
	ength S	Slope	Velocity	Capacity	Description	
(min) (	(teet)	(11/11)	(ft/sec)	(CIS)	Diverse France	
5.0					Direct Entry,	
				Subca	atchment 1.2S:	
				Hydro	graph	
2		.28 cfs			NY-Beacon 24-hr S0P 10-yr Rainfall=4.70'' Runoff Area=0.500 ac	- Runoff
-					Bunoff Volume=0.154 af	
its)					Dupoff Dopth-2'60"	
0) N						
Ë					I C=5.0 min	
1	$-\frac{1}{1}$ $-\frac{1}{1}$ $-\frac{1}{1}$ $-\frac{1}{1}$ $-\frac{1}{1}$	· - <mark> </mark> ¦		$-\frac{1}{1}-\frac{1}{1}-\frac{1}{1}-\frac{1}{1}-\frac{1}{1}-$	+-+-+-+-+-+-+-+-+-+-+-+-+-+-+-+-+-++-++	
					1 <td></td>	
0 2	4 6 8 10	12 14 1	6 18 20 22 24	4 26 28 30 32 3 Tin	34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 me (hours)	

Post Development	NY-Beacon 24-hr S0P	10-yr Rainfall=4.70"
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## Summary for Reach Design Line:

Inflow /	Area	=	26.300 ac,	9.16% Impe	ervious,	Inflow Depth	= 2.3	34" for 10-	yr event
Inflow	=	=	42.97 cfs @	12.34 hrs,	Volume	= 5.13	34 af		
Outflov	V =	=	42.97 cfs @	12.34 hrs,	Volume	= 5.10	34 af,	Atten= 0%,	Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

#### **Reach Design Line:**



#### Summary for Pond 1.1 EDB:

Inflow Area	=	3.300 ac, 5	57.58% Impe	ervious, Inflow	/ Depth =	3.59"	for 10-y	r event	
Inflow =	=	14.74 cfs @	12.03 hrs,	Volume=	0.987	af			
Outflow =	=	4.93 cfs @	12.24 hrs,	Volume=	0.955	af, Atte	n= 67%,	Lag= 12	2.3 min
Primary =	=	0.12 cfs @	12.24 hrs,	Volume=	0.499	af			
Secondary =	=	4.82 cfs @	12.24 hrs,	Volume=	0.456	af			

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 185.85' @ 12.24 hrs Surf.Area= 8,799 sf Storage= 19,626 cf

Plug-Flow detention time= 801.7 min calculated for 0.955 af (97% of inflow) Center-of-Mass det. time= 782.3 min (1,578.4 - 796.1)

Volume	Invert	Avail.Stor	rage Storage	Description	
#1	183.00'	30,70	00 cf Custom	Stage Data (Pr	ismatic) Listed below (Recalc)
Elevatio (fee	on Su et)	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
183.0	0	5,000	0	0	
184.0	00	6,300	5,650	5,650	
186.0	00	9,000	15,300	20,950	
187.0	00	10,500	9,750	30,700	
Device	Routing	Invert	Outlet Device	S	
#1	Primary	182.00'	<b>4.0" Round (</b> L= 40.0' CPF Inlet / Outlet I n= 0.013 Cor	<b>Culvert</b> P, square edge I nvert= 182.00' / rugated PE, sm	neadwall, Ke= 0.500 181.50' S= 0.0125 '/' Cc= 0.900 ooth interior, Flow Area= 0.09 sf
#2	Device 1	182.00'	1.5" Vert. Ori	fice/Grate C=	0.600
#3	Secondary	183.00'	<b>24.0'' Round</b> L= 50.0' CPF Inlet / Outlet I n= 0.013 Cor	<b>Culvert</b> P, square edge h nvert= 183.00' / rugated PE_sm	neadwall, Ke= 0.500 182.00' S= 0.0200 '/' Cc= 0.900 ooth interior Flow Area= 3.14 sf
#4	Device 3	185.50'	<b>8.0' long x 0.</b> Head (feet) 0 Coef. (English	<b>5' breadth Broa</b> 20 0.40 0.60 1) 2.80 2.92 3.	ad-Crested Rectangular Weir 0.80 1.00 08 3.30 3.32
Primary 1=Cu 2=	OutFlow M Ilvert (Pass Orifice/Grat	lax=0.11 cfs ( es 0.11 cfs of ae (Orifice Co	2 12.24 hrs H 0.53 cfs potent ntrols 0.11 cfs	W=185.85' (Fre tial flow) @ 9.37 fps)	ee Discharge)
<u> </u>	<b>A</b>				

Secondary OutFlow Max=4.77 cfs @ 12.24 hrs HW=185.85' (Free Discharge) 3=Culvert (Passes 4.77 cfs of 20.57 cfs potential flow) 4=Broad-Crested Rectangular Weir (Weir Controls 4.77 cfs @ 1.71 fps)

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Pond 1.1 EDB:

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Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
183.00	5,000	0	185.60	8,460	17,458
183.05	5,065	252	185.65	8,528	17,883
183.10	5,130	506	185.70	8,595	18,311
183.15	5,195	765	185.75	8,663	18,742
183.20	5,260	1,026	185.80	8,730	19,177
183.25	5,325	1,291	185.85	8,797	19,615
183.30	5,390	1,559	185.90	0,000 8 032	20,057
183.40	5 520	2 104	186.00	9,000	20,502
183.45	5,585	2,382	186.05	9.075	21,402
183.50	5,650	2,663	186.10	9,150	21,857
183.55	5,715	2,947	186.15	9,225	22,317
183.60	5,780	3,234	186.20	9,300	22,780
183.65	5,845	3,525	186.25	9,375	23,247
183.70	5,910	3,818	186.30	9,450	23,/18
183.75	5,975	4,116	186.35	9,525	24,192
183.85	6 105	4,410	186.45	9,000	24,070
183.90	6,170	5.027	186.50	9,750	25,638
183.95	6,235	5,337	186.55	9,825	26,127
184.00	6,300	5,650	186.60	9,900	26,620
184.05	6,368	5,967	186.65	9,975	27,117
184.10	6,435	6,287	186.70	10,050	27,617
184.15	6,503	6,610	186.75	10,125	28,122
184.20	6,570	6,937 7 267	186.80	10,200	28,030
184.25	6 705	7,207	186.90	10,275	29,142
184.35	6,772	7,938	186.95	10,000	30,177
184.40	6,840	8,278	187.00	10,500	30,700
184.45	6,907	8,622			
184.50	6,975	8,969			
184.55	7,043	9,319			
184.60	7,110	9,673			
184.65	7,178	10,030			
184.70	7,245	10,391			
184.80	7,380	11,122			
184.85	7,447	11,493			
184.90	7,515	11,867			
184.95	7,582	12,244			
185.00	7,650	12,625			
185.05	7,718	13,009			
100.10	7,700	13,397			
185 20	7,000	14 182			
185.25	7,988	14.580			
185.30	8,055	14,981			
185.35	8,122	15,385			
185.40	8,190	15,793			
185.45	8,257	16,204			
185.50	8,325	16,619			
165.55	0,090	17,037			

#### Stage-Area-Storage for Pond 1.1 EDB:

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#### Summary for Pond 1.1 INF:

Inflow Are Inflow Outflow Discardec Primary	a = ( = ( = ( = (	3.300 ac, 57.3 ).12 cfs @ 12 ).10 cfs @ 4 ).10 cfs @ 4 ).00 cfs @ (	58% Impervious, 2.24 hrs, Volume 1.09 hrs, Volume 1.09 hrs, Volume 0.00 hrs, Volume	Inflow Depth >     ≥=   0.499     ≥=   0.496     ≥=   0.496     ≥=   0.000	1.81" for 10-yr event af af, Atten= 16%, Lag= 1,731.1 min af af		
Routing by Peak Elev	Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 180.37' @ 41.09 hrs Surf.Area= 4,150 sf Storage= 1,472 cf						
Plug-Flow Center-of-	detention Mass det.	time= 169.9 n time= 156.9 n Avail Stor	nin calculated for nin ( 2,387.1 - 2,2	0.496 af (99% o 230.3 ) escription	f inflow)		
#1	180.00	16 15	50 cf Custom S	tage Data (Price	natic) Listed below (Becalc)		
πı	100.00	10,10		lage Data (FIISI	natic) Listed below (needle)		
Elevation	S	urf.Area	Inc.Store	Cum.Store			
(feet)		(sq-ft)	(cubic-feet)	(cubic-feet)			
180.00	)	3,750	0	0			
182.00	)	5.900	9,650	9 650			
		- )	0,000	5,050			
183.00	)	7,100	6,500	16,150			
183.00 Device	Routing	7,100 Invert	6,500 Outlet Devices	16,150			
183.00 Device   #1	Routing Discarded	7,100 Invert 180.00'	6,500 Outlet Devices 1.000 in/hr Exfi	16,150	rizontal area		
183.00 <u>Device</u> #1   #2	Routing Discarded Primary	7,100 Invert 180.00' 182.00'	6,500 Outlet Devices 1.000 in/hr Exfi 4.0' long x 0.5'	16,150 Itration over Ho breadth Broad-	rizontal area Crested Rectangular Weir		
183.00 <u>Device</u>   #1   #2	Routing Discarded Primary	7,100 Invert 180.00' 182.00'	6,500 Outlet Devices 1.000 in/hr Exfi 4.0' long x 0.5' Head (feet) 0.2	16,150 Itration over Ho breadth Broad- 0 0.40 0.60 0.8	rizontal area Crested Rectangular Weir 30 1.00		

**Discarded OutFlow** Max=0.10 cfs @ 41.09 hrs HW=180.37' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.10 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=180.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 1.1 INF:



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#### Stage-Area-Storage for Pond 1.1 INF:

Elevation	Surface	Horizontal	Storage
(teet)	(sq-ft)	(sq-ft)	(cubic-feet)
180.00	3,750	3,750	0
180.10	3,857	3,857	380
180.20	3,965	3,965	771
180.30	4,073	4,073	1,173
180.40	4,180	4,180	1,586
180.50	4,288	4,288	2,009
180.60	4,395	4,395	2,443
180.70	4,502	4,502	2,888
180.80	4,610	4,610	3,344
180.90	4,718	4,718	3,810
181.00	4,825	4,825	4,288
181.10	4,932	4,932	4,775
181.20	5,040	5,040	5,274
181.30	5,148	5,148	5,783
181.40	5,255	5,255	6,304
181.50	5,363	5,363	6,834
181.60	5,470	5,470	7,376
181.70	5,577	5,577	7,928
181.80	5,685	5,685	8,492
181.90	5,793	5,793	9,065
182.00	5,900	5,900	9,650
182.10	6,020	6,020	10,246
182.20	6,140	6,140	10,854
182.30	6,260	6,260	11,474
182.40	6,380	6,380	12,106
182.50	6,500	6,500	12,750
182.60	6,620	6,620	13,406
182.70	6,740	6,740	14,074
182.80	6,860	6,860	14,754
182.90	6,980	6,980	15,446
183.00	7,100	7,100	16,150

#### Summary for Pond 1.2 FS:

Inflow Area	=	0.500 ac, 6	2.00% Impe	ervious, Inflow De	epth = 3.6	9" for 10-y	yr event
Inflow =	=	2.28 cfs @	12.03 hrs,	Volume=	0.154 af		
Outflow =	=	2.28 cfs @	12.03 hrs,	Volume=	0.154 af,	Atten= 0%,	Lag= 0.0 min
Primary =	=	1.45 cfs @	12.03 hrs,	Volume=	0.146 af		
Secondary =	=	0.83 cfs @	12.03 hrs,	Volume=	0.008 af		

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 187.48' @ 12.03 hrs Flood Elev= 189.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	186.40'	<b>8.0'' Round Culvert</b> L= 20.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 186.40' / 185.80' S= 0.0300 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Secondary	186.40'	<b>12.0" Round Culvert</b> L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 186.40' / 185.50' S= 0.0180 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#3	Device 2	187.30'	<b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=1.44 cfs @ 12.03 hrs HW=187.47' (Free Discharge) ←1=Culvert (Inlet Controls 1.44 cfs @ 4.13 fps)

Secondary OutFlow Max=0.77 cfs @ 12.03 hrs HW=187.47' (Free Discharge) 2=Culvert (Passes 0.77 cfs of 2.85 cfs potential flow) 3=Broad-Crested Rectangular Weir (Weir Controls 0.77 cfs @ 1.15 fps)

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Pond 1.2 FS:



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Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
186.40	0	187.44	0	188.48	0
186.42	0	187.46	Õ	188.50	0 0
186.44	0	187.48	0	188.52	0
186.46	Õ	187.50	Õ	188.54	0 0
186 48	0 0	187.52	Õ	188.56	0 0
186.50	Õ	187.54	Õ	188.58	0 0
186.52	0 0	187.56	Õ	188.60	0 0
186.54	Õ	187.58	Õ	188.62	0 0
186.56	0	187.60	0	188.64	0
186.58	0	187.62	0	188.66	0
186.60	0	187.64	0	188.68	0
186.62	0	187.66	0	188.70	0
186.64	0	187.68	0	188.72	0
186.66	0	187.70	0	188.74	0
186.68	0	187.72	0	188.76	0
186.70	0	187.74	0	188.78	0
186.72	0	187.76	0	188.80	0
186.74	0	187.78	0	188.82	0
186.76	0	187.80	0	188.84	0
186.78	0	187.82	0	188.86	0
186.80	0	187.84	0	188.88	0
186.82	0	187.86	0	188.90	0
186.84	0	187.88	0	188.92	0
186.86	0	187.90	0	188.94	0
186.88	0	187.92	0	188.96	0
186.90	0	187.94	0	188.98	0
186.92	0	187.96	0	189.00	0
186.94	0	187.98	0		
186.96	0	188.00	0		
186.98	0	188.02	0		
187.00	0	188.04	0		
107.02	0	100.00	0		
107.04	0	100.00	0		
107.00	0	100.10	0		
187.00	0	100.12	0		
187.10	0	188 16	0		
187.12	0	188 18	0		
187 16	0	188.20	0		
187.18	0	188.22	0		
187.20	0	188 24	0		
187.20	0	188.26	0		
187.24	Õ	188.28	Õ		
187.26	0 0	188.30	0 0		
187.28	0 0	188.32	0 0		
187.30	0	188.34	0		
187.32	Ő	188.36	Ő		
187.34	0	188.38	0		
187.36	0	188.40	0		
187.38	0	188.42	0		
187.40	0	188.44	0		
187.42	0	188.46	0		

#### Stage-Area-Storage for Pond 1.2 FS:

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#### Summary for Pond 1.2 INF:

Inflow Area	ι =	0.500 ac, 6	2.00% Impe	ervious, Inflow	Depth = 3	.50" for	10-yr event	
Inflow	=	1.45 cfs @	12.03 hrs,	Volume=	0.146 af			
Outflow	=	0.93 cfs @	12.21 hrs,	Volume=	0.146 af	, Atten= 3	6%, Lag= 1	0.9 min
Discarded	=	0.03 cfs @	8.00 hrs,	Volume=	0.086 af			
Primary	=	0.90 cfs @	12.21 hrs,	Volume=	0.060 af			

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 186.41' @ 12.21 hrs Surf.Area= 0.028 ac Storage= 0.053 af

Plug-Flow detention time= 407.0 min calculated for 0.146 af (100% of inflow) Center-of-Mass det. time= 407.5 min (1,203.1 - 795.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	183.50'	0.026 af	39.50'W x 30.92'L x 3.50'H Field A
			0.098 af Overall - 0.034 af Embedded = 0.064 af x 40.0% Voids
#2A	184.00'	0.034 af	ADS_StormTech SC-740 x 32 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 8 rows
		0 060 of	Total Available Storage

0.060 af Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	183.50'	1.000 in/hr Exfiltration over Horizontal area
#2	Primary	185.80'	8.0" Round Culvert
	-		L= 10.0' CPP, square edge headwall, Ke= 0.500
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf

**Discarded OutFlow** Max=0.03 cfs @ 8.00 hrs HW=183.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.88 cfs @ 12.21 hrs HW=186.41' (Free Discharge) -2=Culvert (Inlet Controls 0.88 cfs @ 2.65 fps)

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Pond 1.2 INF:



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Elevation (feet)	Horizontal (acres)	Storage	Elevation (feet)	Horizontal (acres)	Storage (acre-feet)
183 50	0.028	0.000	186 10	0.028	0.049
183 55	0.028	0.000	186 15	0.028	0.050
183.60	0.028	0.001	186.20	0.028	0.050
183.65	0.028	0.002	186.25	0.028	0.051
183.70	0.028	0.002	186.30	0.028	0.052
183.75	0.028	0.003	186.35	0.028	0.052
183.80	0.028	0.003	186.40	0.028	0.053
183.85	0.028	0.004	186.45	0.028	0.054
183.90	0.028	0.004	186.50	0.028	0.054
183.95	0.028	0.005	186.55	0.028	0.055
184.00	0.028	0.006	186.60	0.028	0.055
184.05	0.028	0.007	186.65	0.028	0.056
184.10	0.028	0.008	186.70	0.028	0.056
184.15	0.028	0.009	186.75	0.028	0.057
184.20	0.028	0.010	186.80	0.028	0.058
184.25	0.028	0.011	186.85	0.028	0.058
184.30	0.028	0.012	186.90	0.028	0.059
184.33	0.028	0.014	187.00	0.028	0.039
184 45	0.020	0.016	107.00	0.020	0.000
184.50	0.028	0.017			
184.55	0.028	0.018			
184.60	0.028	0.019			
184.65	0.028	0.020			
184.70	0.028	0.021			
184.75	0.028	0.023			
184.80	0.028	0.024			
184.85	0.028	0.025			
184.90	0.028	0.026			
184.90	0.028	0.027			
185.00	0.020	0.020			
185 10	0.020	0.020			
185.15	0.028	0.031			
185.20	0.028	0.032			
185.25	0.028	0.033			
185.30	0.028	0.034			
185.35	0.028	0.035			
185.40	0.028	0.036			
185.45	0.028	0.037			
185.50	0.028	0.038			
185.55	0.028	0.039			
100.00	0.028	0.040			
185 70	0.020 0.028	0.041			
185.75	0.020	0.042			
185.80	0.028	0.040			
185.85	0.028	0.045			
185.90	0.028	0.046			
185.95	0.028	0.046			
186.00	0.028	0.047			
186.05	0.028	0.048			

#### Stage-Area-Storage for Pond 1.2 INF:

Post Development	NY-Beacon 24-hr S0P	100-yr Rainfall=8.31"
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## Summary for Subcatchment 1.0S:

Runoff = 81.88 cfs @ 12.35 hrs, Volume= 10.647 af, Depth= 5.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 100-yr Rainfall=8.31"

_	Area	(ac) C	N Desc	cription					
	8.	900 7	'8 Mea	dow, non-g	grazed, HS	G D			
	13.	400 7	'7 Woo	ds, Good,	HSG D				
	0.	200 9	8 Pave	ed parking	, HSG D				
_	22.500 78 Weighted Average								
	22.300 99.11% Pervious Area								
0.200 0.89% Impervious Area									
				•					
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	13.9	100	0.0600	0.12		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 3.16"			
	4.7	345	0.0600	1.22		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	1.4	170	0.0800	1.98		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	3.1	280	0.0900	1.50		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	0.5	225		7.50		Direct Entry, Channel Flow			
	0.0	36				Direct Entry, Pipe Flow			
	0.5	360		12.00		Direct Entry, Channel Flow			
	4.3	30	0.1000	0.12		Sheet Flow,			
_						Woods: Light underbrush n= 0.400 P2= 3.16"			
			-						

28.4 1,546 Total

Post Development	NY-Beacon 24-hr S0P	100-yr Rainfall=8.31"
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Subcatchment 1.0S:



Post Development	NY-Beacon 24-hr S0P	100-yr Rainfall=8.31"
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#### Summary for Subcatchment 1.1S:

Runoff 24.59 cfs @ 12.03 hrs, Volume= 1.955 af, Depth= 7.11" \_

18-

16

12-

10-8-6-

Flow (cfs) 14

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 100-yr Rainfall=8.31"

Area (ac)	CN	Description		
1.900	98	Paved parking	, HSG D	
1.400	80	>75% Grass c	over, Good	I, HSG D
3.300	90	Weighted Aver	rage	
1.400		42.42% Pervio	us Area	
1.900		57.58% Imperv	vious Area	
Tc Leng	gth S	Slope Velocity	Capacity	Description
	ei)		(013)	Direct Entry
5.0				Direct Entry,
			Subca	atchment 1.1S:
			Hydro	ograph
0				
26	-    - <mark>24</mark>	.59 cfs		
24	-      - 			NY-Beacon 24-br S0P 100-vr
22				
20				
				Runoff Area=3.300 ac

Runoff Volume=1.955 af

Runoff Depth=7.11"

Tc=5.0 min

CN=90



Post Development	NY-Beacon 24-hr S0P	100-yr Rainfall=8.31"
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## Summary for Subcatchment 1.2S:

Runoff = 3.76 cfs @ 12.03 hrs, Volume= 0.301 af, Depth= 7.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NY-Beacon 24-hr S0P 100-yr Rainfall=8.31"

(ac) Cl	N Desc	cription		
310 98	8 Pave	ed parking	, HSG D	
190 8	0 >75%	% Grass c	over, Good	, HSG D
500 9	1 Weig	ghted Avei	rage	
190	38.0	0% Pervio	us Area	
310	62.0	0% Imperv	vious Area	
1 11.	01		0	Description
Length (foot)	510pe			Description
(1661)	(11/11)	(11/560)	(015)	Diroot Entry
				Direct Lifti y;
			Subca	atchment 1.2S:
			Hydro	ograph
	3.76 cfs			
				NY-Beacon 24-hr S0P 100-yr
				Bainfall-8 31"
 	 !!	 		
				Runoli Area=0.500 ac
				Runoff Volume=0.301 af
				Runoff Depth=7.23"
	· -		- + - + - + - + -	
				CN_01
·				
		+		
2468	10 12 14 1	16 18 20 22 2	4 26 28 30 3 <u>2</u>	34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72
	(ac) Cr 310 94 190 84 500 9 190 310 Length (feet)	(ac) CN Desc 310 98 Pave 190 80 >755 500 91 Weiq 190 38.0 310 62.0 Length Slope (feet) (ft/ft) 3.76 cfs 3.76 cfs 3.76 cfs 4.6 8 10 12 14 5	(ac)     CN     Description       310     98     Paved parking       190     80     >75% Grass c       500     91     Weighted Aver       190     38.00% Pervio       310     62.00% Impervio       310     62.00% Impervio       Length     Slope     Velocity       (feet)     (ft/ft)     (ft/sec)	(ac)   CN   Description     310   98   Paved parking, HSG D     190   80   >75% Grass cover, Good     500   91   Weighted Average     190   38.00% Pervious Area     310   62.00% Impervious Area     Length   Slope   Velocity   Capacity     (feet)   (ft/ft)   (ft/sec)   (cfs)
Post Development	NY-Beacon 24-hr S0P 10	00-yr Rainfall=8.31"		
---	------------------------	----------------------		
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#### Summary for Reach Design Line:

Inflow /	Area	a =	26.300 ac,	9.16% Impervious,	Inflow Depth = 5.	59" for 100-yr event
Inflow		=	91.95 cfs @	12.32 hrs, Volume	= 12.260 af	
Outflov	v	=	91.95 cfs @	12.32 hrs, Volume	= 12.260 af,	Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

#### **Reach Design Line:**



#### Summary for Pond 1.1 EDB:

Inflow Area	=	3.300 ac, 5	7.58% Impe	ervious,	Inflow Depth =	= 7.1	l1" for	100-	yr event
Inflow	=	24.59 cfs @	12.03 hrs,	Volume	= 1.95	5 af			
Outflow	=	20.62 cfs @	12.09 hrs,	Volume	= 1.92	3 af,	Atten=	16%,	Lag= 3.9 min
Primary	=	0.12 cfs @	12.09 hrs,	Volume	= 0.51	8 af			
Secondary	=	20.50 cfs @	12.09 hrs,	Volume	= 1.40	5 af			

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 186.34' @ 12.09 hrs Surf.Area= 9,516 sf Storage= 24,134 cf

Plug-Flow detention time= 422.8 min calculated for 1.923 af (98% of inflow) Center-of-Mass det. time= 412.1 min (1,187.3 - 775.2)

Volume	Invert	Avail.Stor	rage Storage	Description		
#1	183.00'	30,70	0 cf Custom	n Stage Data (Pr	ismatic) Listed below (Recalc)	
Elevation (feet)	Su	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
183.00		5,000	0	0		
184.00		6,300	5,650	5,650		
186.00		9,000	15,300	20,950		
187.00		10,500	9,750	30,700		
Device F	Routing	Invert	Outlet Device	es		
#1 F	Primary	182.00'	4.0" Round	Culvert		
			L= 40.0' CP Inlet / Outlet n= 0.013 Co	P, square edge   Invert= 182.00' / rrugated PE, sm	neadwall, Ke= 0.500 181.50' S= 0.0125 '/' Cc= 0.900 ooth interior, Flow Area= 0.09 sf	
#2 [	Device 1	182.00'	1.5" Vert. Ori	ifice/Grate C=	0.600	
#3 \$	Secondary	183.00'	<b>24.0'' Round</b> L= 50.0' CP Inlet / Outlet   n= 0.013 Co	<b>l Culvert</b> P, square edge I Invert= 183.00' / rrugated PE, sm	headwall, Ke= 0.500 182.00' S= 0.0200 '/' Cc= 0.900 ooth interior, Flow Area= 3.14 sf	
#4 [	Device 3	185.50'	<b>8.0' long x 0</b> Head (feet) ( Coef. (Englis	<b>.5' breadth Broa</b> 0.20 0.40 0.60 h) 2.80 2.92 3.	ad-Crested Rectangular Weir 0.80 1.00 .08 3.30 3.32	
Primary OutFlow Max=0.12 cfs @ 12.09 hrs HW=186.34' (Free Discharge) 1=Culvert (Passes 0.12 cfs of 0.56 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.12 cfs @ 9.96 fps)						

Secondary OutFlow Max=20.35 cfs @ 12.09 hrs HW=186.34' (Free Discharge) -3=Culvert (Passes 20.35 cfs of 23.14 cfs potential flow) -4=Broad-Crested Rectangular Weir (Weir Controls 20.35 cfs @ 3.03 fps)

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Pond 1.1 EDB:

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#### Stage-Area-Storage for Pond 1.1 EDB:

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
183.00	5,000	0	185.60	8,460	17,458
183.05	5,065	252	185.65	8,528	17,883
183.10	5,130	506	185.70	8,595	18,311
183.15	5,195	/65	185.75	8,663	18,/42
183.20	5,260	1,026	185.80	8,730	19,177
183.25	5,3∠5 5,200	1,291	185.85	8,797	19,015
103.30	5,390	1,009	185.90	0,000	20,007
183.40	5,400	2 104	186.00	9,000	20,502
183.45	5,585	2,382	186.05	9.075	21,402
183.50	5,650	2,663	186.10	9,150	21,857
183.55	5,715	2,947	186.15	9,225	22,317
183.60	5,780	3,234	186.20	9,300	22,780
183.65	5,845	3,525	186.25	9,375	23,247
183.70	5,910	3,818	186.30	9,450	23,718
183.75	5,975	4,116	186.35	9,525	24,192
183.80	6,040	4,416	186.40	9,600	24,670
183.00	6,105	4,720	186 50	9,675	25,152
183.95	6 235	5 337	186.55	9,825	26,000
184.00	6.300	5.650	186.60	9.900	26.620
184.05	6,368	5,967	186.65	9,975	27,117
184.10	6,435	6,287	186.70	10,050	27,617
184.15	6,503	6,610	186.75	10,125	28,122
184.20	6,570	6,937	186.80	10,200	28,630
184.25	6,638	7,267	186.85	10,275	29,142
184.30	6,705	7,001	186.90	10,350	29,658
184.35	6,772	7,930	187.00	10,425 <b>10 500</b>	<b>30</b> ,177 <b>30 700</b>
184 45	6 907	8 622	107.00	10,500	50,700
184.50	6,975	8,969			
184.55	7,043	9,319			
184.60	7,110	9,673			
184.65	7,178	10,030			
184.70	7,245	10,391			
184.75	7,313	10,755			
184.80	7,380	11,122			
184.00	7,447	11,493			
184.95	7,513	12 244			
185.00	7,650	12.625			
185.05	7,718	13,009			
185.10	7,785	13,397			
185.15	7,853	13,788			
185.20	7,920	14,182			
185.25	7,988	14,580			
185.30	8,055	14,981			
185 /0	0,122 8 100	10,000			
185 45	8 257	16 204			
185.50	8.325	16.619			
185.55	8,393	17,037			
	-				

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#### Summary for Pond 1.1 INF:

Inflow Area	=	3.300 ac, 5	7.58% Impe	ervious, li	nflow Depth >	1.88"	for 100-	yr event	
Inflow	=	0.12 cfs @	12.09 hrs,	Volume=	0.518 a	af			
Outflow	=	0.10 cfs @	40.74 hrs,	Volume=	0.514 a	af, Atter	ı= 21%,	Lag= 1,718.	6 min
Discarded	=	0.10 cfs @	40.74 hrs,	Volume=	0.514 a	af			
Primary	=	0.00 cfs @	0.00 hrs,	Volume=	0.000 a	af			

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 180.39' @ 40.74 hrs Surf.Area= 4,171 sf Storage= 1,549 cf

Plug-Flow detention time= 177.5 min calculated for 0.514 af (99% of inflow) Center-of-Mass det. time= 159.5 min (2,327.9 - 2,168.4)

Volume	Invert	Avail.Stor	age Storage	Description	
#1	180.00'	16,15	0 cf Custom	Stage Data (Pris	smatic) Listed below (Recalc)
Elevatio (fee 180.0	on Su et) 00	urf.Area (sq-ft) 3,750	Inc.Store (cubic-feet) 0	Cum.Store (cubic-feet) 0	
182.( 183.(	00 00	5,900 7,100	9,650 6,500	9,650 16,150	
Device	Routing	Invert	Outlet Device	S	
#1 #2	Discarded Primary	180.00' 182.00'	<b>1.000 in/hr Ex</b> <b>4.0' long x 0.</b> Head (feet) 0 Coef. (English	<b>(filtration over H 5' breadth Broa</b> .20 0.40 0.60 ( n) 2.80 2.92 3.0	orizontal area d-Crested Rectangular Weir ).80 1.00 )8 3.30 3.32
Discard	ed OutFlow	Max=0.10 cfs	s @ 40.74 hrs	HW=180.39' (F	ree Discharge)

**1=Exfiltration** (Exfiltration Controls 0.10 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=180.00' (Free Discharge) ←2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 1.1 INF:



#### Post Development

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#### Stage-Area-Storage for Pond 1.1 INF:

Elevation	Surface	Horizontal	Storage
(feet)	(sq-ft)	(sq-ft)	(cubic-feet)
180.00	3,750	3,750	0
180.10	3,857	3,857	380
180.20	3,965	3,965	771
180.30	4,073	4,073	1,173
180.40	4,180	4,180	1,586
180.50	4,288	4,288	2,009
180.60	4,395	4,395	2,443
180.70	4,502	4,502	2,888
180.80	4,610	4,610	3,344
180.90	4,718	4,718	3,810
181.00	4,825	4,825	4,288
181.10	4,932	4,932	4,775
181.20	5,040	5,040	5,274
181.30	5,148	5,148	5,783
181.40	5,255	5,255	6,304
181.50	5,363	5,363	6,834
181.60	5,470	5,470	7,376
181.70	5,577	5,577	7,928
181.80	5,685	5,685	8,492
181.90	5,793	5,793	9,065
182.00	5,900	5,900	9,650
182.10	6,020	6,020	10,246
182.20	6,140	6,140	10,854
182.30	6,260	6,260	11,474
182.40	6,380	6,380	12,106
182.50	6,500	6,500	12,750
182.60	6,620	6,620	13,406
182.70	6,740	6,740	14,074
182.80	6,860	6,860	14,754
182.90	6,980	6,980	15,446
183.00	7,100	7,100	16,150

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#### Summary for Pond 1.2 FS:

Inflow Area	=	0.500 ac, 6	2.00% Impe	ervious, Inflow D	epth = 7	.23" for 100-yr event
Inflow =	=	3.76 cfs @	12.03 hrs,	Volume=	0.301 af	
Outflow =	=	3.76 cfs @	12.03 hrs,	Volume=	0.301 af	, Atten= 0%, Lag= 0.0 min
Primary =	=	1.59 cfs @	12.03 hrs,	Volume=	0.269 af	-
Secondary =	=	2.17 cfs @	12.03 hrs,	Volume=	0.032 af	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 187.63' @ 12.03 hrs Flood Elev= 189.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	186.40'	<b>8.0'' Round Culvert</b> L= 20.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 186.40' / 185.80' S= 0.0300 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Secondary	186.40'	<b>12.0'' Round Culvert</b> L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 186.40' / 185.50' S= 0.0180 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#3	Device 2	187.30'	<b>4.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=1.58 cfs @ 12.03 hrs HW=187.62' (Free Discharge) -1=Culvert (Inlet Controls 1.58 cfs @ 4.53 fps)

Secondary OutFlow Max=2.08 cfs @ 12.03 hrs HW=187.62' (Free Discharge) 2=Culvert (Passes 2.08 cfs of 3.21 cfs potential flow) 3=Broad-Crested Rectangular Weir (Weir Controls 2.08 cfs @ 1.62 fps)

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Pond 1.2 FS:



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Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
186.40	Ó	187.44		188.48	
186.42	0	187.46	0	188.50	0
186.44	0	187.48	0	188.52	0
186.46	0	187.50	0	188.54	0
186.48	0	187.52	0	188.56	0
186.50	0	187.54	0	188.58	0
186.52	0	187.56	0	188.60	0
186.54	0	187.58	0	188.62	0
186.56	0	187.60	0	188.64	0
186.58	0	187.62	0	188.66	0
186.60	0	187.64	0	188.68	0
186.62	0	187.66	0	188.70	0
186.64	0	187.68	0	188.72	0
	0	187.70	0	188.74	0
100.00	0	107.72	0	100.70	0
100.70	0	107.74	0	100.70	0
186.72	0	187.70	0	188.82	0
186 76	0	187.80	0	188.8/	0
186 78	0	187.82	0	188.86	0
186.80	0	187.84	0	188.88	0
186.82	0	187.86	0	188.90	0
186.84	0 0	187.88	ů 0	188.92	0
186.86	Ő	187.90	ů 0	188.94	Ő
186.88	Ō	187.92	0	188.96	0
186.90	0	187.94	0	188.98	0
186.92	0	187.96	0	189.00	0
186.94	0	187.98	0		
186.96	0	188.00	0		
186.98	0	188.02	0		
187.00	0	188.04	0		
187.02	0	188.06	0		
187.04	0	188.08	0		
187.06	0	188.10	0		
187.08	0	188.12	0		
107.10	0	100.14	0		
107.12	0	100.10	0		
187.14	0	188.20	0		
187.18	0	188 22	0		
187.20	0	188 24	0		
187.22	0	188.26	Ő		
187.24	Ő	188.28	0		
187.26	0	188.30	0		
187.28	0	188.32	0		
187.30	0	188.34	0		
187.32	0	188.36	0		
187.34	0	188.38	0		
187.36	0	188.40	0		
187.38	0	188.42	0		
187.40	0	188.44	0		
187.42	0	188.46	0		

#### Stage-Area-Storage for Pond 1.2 FS:

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#### Summary for Pond 1.2 INF:

Inflow Area	ι =	0.500 ac, 6	2.00% Impe	ervious, Inflow	Depth = 6.4	15" for 100	-yr event
Inflow	=	1.59 cfs @	12.03 hrs,	Volume=	0.269 af		
Outflow	=	1.46 cfs @	12.14 hrs,	Volume=	0.269 af,	Atten= 8%,	Lag= 6.9 min
Discarded	=	0.03 cfs @	5.15 hrs,	Volume=	0.092 af		-
Primary	=	1.44 cfs @	12.14 hrs,	Volume=	0.176 af		

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 186.86' @ 12.14 hrs Surf.Area= 0.028 ac Storage= 0.058 af

Plug-Flow detention time= 244.4 min calculated for 0.269 af (100% of inflow) Center-of-Mass det. time= 245.0 min (1,022.6 - 777.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	183.50'	0.026 af	39.50'W x 30.92'L x 3.50'H Field A
			0.098 af Overall - 0.034 af Embedded = 0.064 af x 40.0% Voids
#2A	184.00'	0.034 af	ADS_StormTech SC-740 x 32 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 8 rows
-		0.060 of	Total Available Storage

0.060 af Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	183.50'	1.000 in/hr Exfiltration over Horizontal area
#2	Primary	185.80'	8.0" Round Culvert
			L= 10.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 185.80' / 185.50' S= 0.0300 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf

**Discarded OutFlow** Max=0.03 cfs @ 5.15 hrs HW=183.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=1.43 cfs @ 12.14 hrs HW=186.86' (Free Discharge) —2=Culvert (Inlet Controls 1.43 cfs @ 4.11 fps)

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Pond 1.2 INF:



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Elevation	Horizontal	Storage	Elevation	Horizontal	Storage
	(acres)	(acre-feet)	(teet)	(acres)	(acre-feet)
183.50	0.028	0.000	186.10	0.028	0.049
183.55	0.028	0.001	186.15	0.028	0.050
183.60	0.028	0.001	186.20	0.028	0.050
183.65	0.028	0.002	186.25	0.028	0.051
183.70	0.028	0.002	186.30	0.028	0.052
183.75	0.028	0.003	186.35	0.028	0.052
183.80	0.028	0.003	186.40	0.028	0.053
183.85	0.028	0.004	186.45	0.028	0.054
183.90	0.028	0.004	186.50	0.028	0.054
183.95	0.028	0.005	186.55	0.028	0.055
184.00	0.028	0.006	186.60	0.028	0.055
184.05	0.028	0.007	186.65	0.028	0.056
184.10	0.028	0.008	186.70	0.028	0.056
184.15	0.028	0.009	186.75	0.028	0.057
184.20	0.028	0.010	186.80	0.028	0.058
184.25	0.028	0.011	186.85	0.028	0.058
184.30	0.028	0.012	186.90	0.028	0.059
184.35	0.028	0.014	186.95	0.028	0.059
184.40	0.028	0.015	187.00	0.028	0.060
184.45	0.028	0.016			
184.50	0.028	0.017			
184.55	0.028	0.018			
184.60	0.028	0.019			
184.65	0.028	0.020			
184.70	0.028	0.021			
184.75	0.028	0.023			
104.00	0.020	0.024			
104.00	0.020	0.025			
104.90	0.020	0.020			
185.00	0.028	0.027			
185.00	0.020	0.020			
185 10	0.020	0.023			
185 15	0.028	0.000			
185 20	0.028	0.001			
185.25	0.028	0.033			
185.30	0.028	0.034			
185.35	0.028	0.035			
185 40	0.028	0.036			
185.45	0.028	0.037			
185.50	0.028	0.038			
185.55	0.028	0.039			
185.60	0.028	0.040			
185.65	0.028	0.041			
185.70	0.028	0.042			
185.75	0.028	0.043			
185.80	0.028	0.044			
185.85	0.028	0.045			
185.90	0.028	0.046			
185.95	0.028	0.046			
186.00	0.028	0.047			
186.05	0.028	0.048			

#### Stage-Area-Storage for Pond 1.2 INF:

#### **APPENDIX D**

#### **Project and Owner information**

#### Site Data:

Beacon Views City of Beacon Dutchess County, New York

#### **Owner Information:**

Highlands @ Beacon, LLC 2847 Church Street Pine Plains, New York 12567

#### Applicant Information:

Beacon Views, LLC 500 River Avenue Wakefield, New Jersey 08701

## Party Responsible for Implementation of the Stormwater Pollution Prevention Plan (Including Maintenance During and After Construction):

Beacon Views, LLC 500 River Avenue Wakefield, New Jersey 08701

#### **Qualified Professional Responsible for Inspection of the Stormwater Pollution Prevention Plan:**

Inspector to be determined at time of construction

#### **APPENDIX E**

NYSDEC SPDES for Construction Activities Construction Site Log Book

### APPENDIX F CONSTRUCTION SITE INSPECTION AND MAINTENANCE LOG BOOK

## STATE POLLUTANT DISCHARGE ELIMINATION SYSTEM FOR CONSTRUCTION ACTIVITIES

### SAMPLE CONSTRUCTION SITE LOG BOOK

#### Table of Contents

- I. Pre-Construction Meeting Documents
  - a. Preamble to Site Assessment and Inspections
  - b. Pre-Construction Site Assessment Checklist

### **II.** Construction Duration Inspections

- a. Directions
- b. Modification to the SWPPP

#### I. PRE-CONSTRUCTION MEETING DOCUMENTS

Project Name	
Permit No.	Date of Authorization
Name of Operator	
Prime Contractor	

#### a. Preamble to Site Assessment and Inspections

The Following Information To Be Read By All Person's Involved in The Construction of Stormwater Related Activities:

The Operator agrees to have a qualified inspector<sup>1</sup> conduct an assessment of the site prior to the commencement of construction<sup>2</sup> and certify in this inspection report that the appropriate erosion and sediment controls described in the SWPPP have been adequately installed or implemented to ensure overall preparedness of the site for the commencement of construction.

Prior to the commencement of construction, the Operator shall certify in this site logbook that the SWPPP has been prepared in accordance with the State's standards and meets all Federal, State and local erosion and sediment control requirements. A preconstruction meeting should be held to review all of the SWPPP requirements with construction personnel.

When construction starts, site inspections shall be conducted by the qualified inspector at least every 7 calendar days. The Operator shall maintain a record of all inspection reports in this site logbook. The site logbook shall be maintained on site and be made available to the permitting authorities upon request.

Prior to filing the Notice of Termination or the end of permit term, the Operator shall have a qualified inspector perform a final site inspection. The qualified inspector shall certify that the site has undergone final stabilization<sup>3</sup> using either vegetative or structural stabilization methods and that all temporary erosion and sediment controls (such as silt fencing) not needed for long-term erosion control have been removed. In addition, the Operator must identify and certify that all permanent structures described in the SWPPP have been constructed and provide the owner(s) with an operation and maintenance plan that ensures the structure(s) continuously functions as designed.

1 Refer to "Qualified Inspector" inspection requirements in the current SPDES General Permit for Stormwater Discharges from Construction Activity for complete list of inspection requirements.

3 "Final stabilization" means that all soil-disturbing activities at the site have been completed and a uniform, perennial vegetative cover with a density of eighty (80) percent has been established or equivalent stabilization measures (such as the use of mulches or geotextiles) have been employed on all unpaved areas and areas not covered by permanent structures.

<sup>2 &</sup>quot;Commencement of construction" means the initial removal of vegetation and disturbance of soils associated with clearing, grading or excavating activities or other construction activities.

#### b. Pre-construction Site Assessment Checklist (NOTE: Provide comments below as necessary)

1. Notice of Intent, SWPPP, and Contractors Certification:

#### Yes No NA

- [] [] Has a Notice of Intent been filed with the NYS Department of Conservation?
- [] [] Is the SWPPP on-site? Where?
- [] [] Is the Plan current? What is the latest revision date?\_\_\_\_\_
- [] [] Is a copy of the NOI (with brief description) onsite? Where?\_\_\_\_
- [] [] Have all contractors involved with stormwater related activities signed a contractor's certification?

#### 2. Resource Protection

#### Yes No NA

- [] [] Are construction limits clearly flagged or fenced?
- [] [] Important trees and associated rooting zones, on-site septic system absorption fields, existing vegetated areas suitable for filter strips, especially in perimeter areas, have been flagged for protection.
- [] [] Creek crossings installed prior to land-disturbing activity, including clearing and blasting.
- 3. Surface Water Protection

#### Yes No NA

- [] [] Clean stormwater runoff has been diverted from areas to be disturbed.
- [] [] Bodies of water located either on site or in the vicinity of the site have been identified and protected.
- [] [] Appropriate practices to protect on-site or downstream surface water are installed.
- [] [] Are clearing and grading operations divided into areas <5 acres?
- 4. Stabilized Construction Access

#### Yes No NA

- [] [] A temporary construction entrance to capture mud and debris from construction vehicles before they enter the public highway has been installed.
- [] [] Other access areas (entrances, construction routes, equipment parking areas) are stabilized immediately as work takes place with gravel or other cover.
- [] [] Sediment tracked onto public streets is removed or cleaned on a regular basis.
- 5. Sediment Controls

#### Yes No NA

- [] [] Silt fence material and installation comply with the standard drawing and specifications.
- [] [] [] Silt fences are installed at appropriate spacing intervals
- [] [] Sediment/detention basin was installed as first land disturbing activity.
- [] [] [] Sediment traps and barriers are installed.

#### 6. Pollution Prevention for Waste and Hazardous Materials

#### Yes No NA

- [] [] The Operator or designated representative has been assigned to implement the spill prevention avoidance and response plan.
- [] [] The plan is contained in the SWPPP on page \_
- [] [] Appropriate materials to control spills are onsite. Where?

#### **II. CONSTRUCTION DURATION INSPECTIONS**

#### a. Directions:

#### Inspection Forms will be filled out during the entire construction phase of the project.

Required Elements:

- 1) On a site map, indicate the extent of all disturbed site areas and drainage pathways. Indicate site areas that are expected to undergo initial disturbance or significant site work within the next 14-day period;
- 2) Indicate on a site map all areas of the site that have undergone temporary or permanent stabilization;
- 3) Indicate all disturbed site areas that have not undergone active site work during the previous 14-day period;
- 4) Inspect all sediment control practices and record the approximate degree of sediment accumulation as a percentage of sediment storage volume (for example, 10 percent, 20 percent, 50 percent);
- 5) Inspect all erosion and sediment control practices and record all maintenance requirements such as verifying the integrity of barrier or diversion systems (earthen berms or silt fencing) and containment systems (sediment basins and sediment traps). Identify any evidence of rill or gully erosion occurring on slopes and any loss of stabilizing vegetation or seeding/mulching. Document any excessive deposition of sediment or ponding water along barrier or diversion systems. Record the depth of sediment within containment structures, any erosion near outlet and overflow structures, and verify the ability of rock filters around perforated riser pipes to pass water; and
- 6) Immediately report to the Operator any deficiencies that are identified with the implementation of the SWPPP.

#### SITE PLAN/SKETCH

 Inspector (print name)
 Date of Inspection

 Qualified Inspector (print name)
 Qualified Inspector Signature

The above signed acknowledges that, to the best of his/her knowledge, all information provided on the forms is accurate and complete.

#### CONSTRUCTION DURATION INSPECTIONS

#### **Maintaining Water Quality**

#### Yes No NA

- [] [] Is there an increase in turbidity causing a substantial visible contrast to natural conditions at the outfalls?
- [] [] Is there residue from oil and floating substances, visible oil film, or globules or grease at the outfalls?
- [] [] All disturbance is within the limits of the approved plans.
- [] [] Have receiving lake/bay, stream, and/or wetland been impacted by silt from project?

#### Housekeeping

1. General Site Conditions

#### Yes No NA

- [] [] [] Is construction site litter, debris and spoils appropriately managed?
- [] [] [] Are facilities and equipment necessary for implementation of erosion and sediment control in working order and/or properly maintained?
- [] [] [] Is construction impacting the adjacent property?
- [] [] [] Is dust adequately controlled?

#### 2. Temporary Stream Crossing

#### Yes No NA

- [] [] Maximum diameter pipes necessary to span creek without dredging are installed.
- [] [] Installed non-woven geotextile fabric beneath approaches.
- [] [] Is fill composed of aggregate (no earth or soil)?
- [] [] Rock on approaches is clean enough to remove mud from vehicles & prevent sediment from entering stream during high flow.
- 3. Stabilized Construction Access

#### Yes No NA

- [] [] Stone is clean enough to effectively remove mud from vehicles.
- [] [] [] Installed per standards and specifications?
- [] [] Does all traffic use the stabilized entrance to enter and leave site?
- [] [] [] Is adequate drainage provided to prevent ponding at entrance?

#### **Runoff Control Practices**

1. Excavation Dewatering

#### Yes No NA

- [] [] Upstream and downstream berms (sandbags, inflatable dams, etc.) are installed per plan.
- [] [] Clean water from upstream pool is being pumped to the downstream pool.
- [] [] Sediment laden water from work area is being discharged to a silt-trapping device.
- [] [] Constructed upstream berm with one-foot minimum freeboard.

#### **Runoff Control Practices (continued)**

#### 2. Flow Spreader

#### Yes No NA

- [] [] [] Installed per plan.
- [] [] Constructed on undisturbed soil, not on fill, receiving only clear, non-sediment laden flow.
- [] [] Flow sheets out of level spreader without erosion on downstream edge.

#### 3. Interceptor Dikes and Swales

#### Yes No NA

- [] [] [] Installed per plan with minimum side slopes 2H:1V or flatter.
- [] [] Stabilized by geotextile fabric, seed, or mulch with no erosion occurring.
- [] [] [] Sediment-laden runoff directed to sediment trapping structure

#### 4. Stone Check Dam

#### Yes No NA

- [] [] [] Is channel stable? (flow is not eroding soil underneath or around the structure).
- [] [] Check is in good condition (rocks in place and no permanent pools behind the structure).
- [] [] Has accumulated sediment been removed?.

#### 5. Rock Outlet Protection

#### Yes No NA

- [] [] [] Installed per plan.
- [] [] Installed concurrently with pipe installation.

#### Soil Stabilization

1. Topsoil and Spoil Stockpiles

#### Yes No NA

- [] [] [] Stockpiles are stabilized with vegetation and/or mulch.
- [] [] Sediment control is installed at the toe of the slope.

#### 2. Revegetation

#### Yes No NA

- [] [] [] Temporary seedings and mulch have been applied to idle areas.
- [] [] 4 inches minimum of topsoil has been applied under permanent seedings

#### Sediment Control Practices

1. Silt Fence and Linear Barriers

#### Yes No NA

- [] [] Installed on Contour, 10 feet from toe of slope (not across conveyance channels).
- [] [] Joints constructed by wrapping the two ends together for continuous support.
- [] [] Fabric buried 6 inches minimum.
- [] [] Posts are stable, fabric is tight and without rips or frayed areas.

Sediment accumulation is \_\_\_% of design capacity.

#### CONSTRUCTION DURATION INSPECTIONS

Page 4 of \_\_\_\_\_

#### Sediment Control Practices (continued)

2. Storm Drain Inlet Protection (Use for Stone & Block; Filter Fabric; Curb; or, Excavated; Filter Sock or Manufactured practices)

#### Yes No NA

- [] [] Installed concrete blocks lengthwise so open ends face outward, not upward.
- [] [] Placed wire screen between No. 3 crushed stone and concrete blocks.
- [] [] Drainage area is 1acre or less.
- [] [] [] Excavated area is 900 cubic feet.
- [] [] Excavated side slopes should be 2:1.
- [] [] 2" x 4" frame is constructed and structurally sound.
- [] [] Posts 3-foot maximum spacing between posts.
- [] [] Fabric is embedded 1 to 1.5 feet below ground and secured to frame/posts with staples at max 8-inch spacing.
- [] [] Posts are stable, fabric is tight and without rips or frayed areas.
- [] [] [] Manufactured insert fabric is free of tears and punctures.
- [] [] Filter Sock is not torn or flattened and fill material is contained within the mesh sock.

Sediment accumulation \_\_\_% of design capacity.

3. Temporary Sediment Trap

#### Yes No NA

- [] [] Outlet structure is constructed per the approved plan or drawing.
- [] [] Geotextile fabric has been placed beneath rock fill.
- [] [] Sediment trap slopes and disturbed areas are stabilized.

Sediment accumulation is \_\_\_% of design capacity.

4. Temporary Sediment Basin

#### Yes No NA

- [] [] Basin and outlet structure constructed per the approved plan.
- [] [] Basin side slopes are stabilized with seed/mulch.
- [] [] Drainage structure flushed and basin surface restored upon removal of sediment basin facility.
- [] [] Sediment basin dewatering pool is dewatering at appropriate rate.

Sediment accumulation is \_\_\_% of design capacity.

<u>Note</u>: Not all erosion and sediment control practices are included in this listing. Add additional pages to this list as required by site specific design. All practices shall be maintained in accordance with their respective standards.

Construction inspection checklists for post-development stormwater management practices can be found in Appendix F of the New York Stormwater Management Design Manual.

#### CONSTRUCTION DURATION INSPECTIONS

#### **b.** Modifications to the SWPPP (To be completed as described below)

The Operator shall amend the SWPPP whenever:

- 1. There is a significant change in design, construction, operation, or maintenance which may have a significant effect on the potential for the discharge of pollutants to the waters of the United States and which has not otherwise been addressed in the SWPPP; or
- 2. The SWPPP proves to be ineffective in:
  - a. Eliminating or significantly minimizing pollutants from sources identified in the SWPPP and as required by this permit; or
  - b. Achieving the general objectives of controlling pollutants in stormwater discharges from permitted construction activity; and
- 3. Additionally, the SWPPP shall be amended to identify any new contractor or subcontractor that will implement any measure of the SWPPP.

#### **Modification & Reason:**

#### **APPENDIX F**

#### NYSDEC Stormwater Design Manual Chapter 5 Analysis

Table Key:

• = Practice Used in Accordance with Chapter 5 Requirements

- o = Practice Not Used
- = Practice is Not Applicable

	Subcat	chments	Domorko
NTSDEC Chapter 5 Requirements	1.1	1.2	nemarks
Chapter 5, Section 5.1: Preserva	ation if Natural	Features and Co	nservation Design
Practices			
Preservation of Undisturbed Areas	•	•	See Note #2
Preservation of Buffers	-	-	
Reduction of Clearing & Grading	•	•	See Note #4
Locating Development in Less Sensitive Areas	•	•	See Note #4
Open Space Design	-	-	
Soil Restoration	•	•	See Note #5
Chapter 5, Section	5.2: Reduction	of Impervious C	over
Practices			
Roadway Reduction	-	-	
Sidewalk Reduction	•	•	
Driveway Reduction	•	•	See Note #1
Cul-de-sac Reduction	-	-	
Building Footprint Reduction	•	•	See Note #3
Parking Reduction	•	•	See Note #4
Conservation of Natural Areas	-	-	See Note #2
Sheetflow to Riparian Buffers or Filter Strips	-	-	
Vegetated Swale	•	•	
Tree Planting / Tree Pit	-	-	
Disconnection of Rooftop Runoff	-	-	
Stream Daylighting	-	-	
Rain Gardens	-	-	
Green Roofs	-	-	
Stormwater Planters	-	-	
Rain Barrels / Cisterns	-	-	
Porous Pavement	-	-	

Notes:

- 1. The proposed driveway entrance has been designed to provide a minimum width for safe ingress and egress for the development.
- 2. Although no formal calculations have been provided, the subject project has provided conservation of natural areas to the maximum extent practical.
- 3. The proposed buildings are multi-story, thus minimize the building footprints.
- 4. The reduction in clearing and grading, as well as the driveway and parking areas foot print reduction will be enforced with the approval of the project PSWPPP. Notes on the project plans, establish that any changes in the project plans would require an amended approval from the necessary regulatory agencies
- 5. Soil restoration requirements per NYSDEC stantards shown on project plans.

#### **APPENDIX G**

NYSDEC Infiltration Construction and Maintenance Inspection Checklist

### **Infiltration Trench Construction Inspection Checklist**

Project: Location: Site Status:

Date:

Time:

Inspector:

CONSTRUCTION SEQUENCE	Satisfactory/ Unsatisfactory	Comments		
1. Pre-Construction				
Pre-construction meeting				
Runoff diverted				
Soil permeability tested				
Groundwater / bedrock sufficient at depth				
2. Excavation				
Size and location				
Side slopes stable				
Excavation does not compact subsoils				
3. Filter Fabric Placement				
Fabric specifications				
Placed on bottom, sides, and top				

CONSTRUCTION SEQUENCE	SATISFACTORY / UNSATISFACTORY	Comments			
4. Aggregate Material					
Size as specified					
Clean / washed material					
Placed properly					
5. Observation Well					
Pipe size					
Removable cap / footplate					
Initial depth =feet					
6. Final Inspection					
Pretreatment facility in place					
Contributing watershed stabilized prior to flow diversion					
Outlet					

#### Comments:



#### Actions to be Taken:
Project:

5. Inlets

(Annual)

## Infiltration Trench Operation, Maintenance, and Management Inspection Checklist

Site Status:		
Date:		
Time:		
Inspector:		
MAINTENANCE ITEM	SATISFACTORY / UNSATISFACTORY	COMMENTS
1. Debris Cleanout (Monthly	()	
Trench surface clear of debris		
Inflow pipes clear of debris		
Overflow spillway clear of debris		
Inlet area clear of debris		
2. Sediment Traps or Forebays (A	nnual)	
Obviously trapping sediment		
Greater than 50% of storage volume remaining		
3. Dewatering (Monthly)		
Trench dewaters between storms		
4. Sediment Cleanout of Trench	(Annual)	
No evidence of sedimentation in trench		
Sediment accumulation doesn't yet require cleanout		

Maintenance Item	Satisfactory / Unsatisfactory	Comments
Good condition		
No evidence of erosion		
6. Outlet/Overflow Spillway (Annua	I)	
Good condition, no need for repair		
No evidence of erosion		
7. Aggregate Repairs (Annual)		
Surface of aggregate clean		
Top layer of stone does not need replacement		
Trench does not need rehabilitation		

### Comments:

## Actions to be Taken:

# **Infiltration Basin Construction Inspection Checklist**

Project: Location: Site Status:

Date:

Time:

Inspector:

CONSTRUCTION SEQUENCE	Satisfactory/ Unsatisfactory	COMMENTS
1. Pre-Construction		
Runoff diverted		
Soil permeability tested		
Groundwater / bedrock depth		
2. Excavation		
Size and location		
Side slopes stable		
Excavation does not compact subsoils		
3. Embankment		
Barrel		
Anti-seep collar or Filter diaphragm		
Fill material		

CONSTRUCTION SEQUENCE	Satisfactory/ Unsatisfactory	COMMENTS
4. Final Excavation		
Drainage area stabilized		
Sediment removed from facility		
Basin floor tilled		
Facility stabilized		
5. Final Inspection		
Pretreatment facility in place		
Inlets / outlets		
Contributing watershed stabilized before flow is routed to the factility		

## Comments:

## Actions to be Taken:

## **APPENDIX H**

Hydrodynamic Separator Sizing and Maintenance Manual



## State of New Jersey

PHILIP D. MURPHY Governor

SHEILA Y. OLIVER Lt. Governor DEPARTMENT OF ENVIRONMENTAL PROTECTION Mail Code – 401-02B Division of Water Quality Bureau of Nonpoint Pollution Control P.O. Box 420 – 401 E. State St. Trenton, NJ 08625-0420 Phone: (609) 633-7021 / Fax: (609) 777-0432 http://www.state.nj.us/dep/dwq/bnpc\_home.htm

CATHERINE R. MCCABE Acting Commissioner

March 27, 2018

Graham Bryant, M.Sc., P.E. President Hydroworks, LLC 136 Central Avenue Clark, NJ 07066

Re: MTD Lab Certification HydroStorm Hydrodynamic Separator by Hydroworks, LLC Online Installation

#### TSS Removal Rate 50%

Dear Mr. Bryant:

The Stormwater Management rules under N.J.A.C. 7:8-5.5(b) and 5.7 (c) allow the use of manufactured treatment devices (MTDs) for compliance with the design and performance standards at N.J.A.C. 7:8-5 if the pollutant removal rates have been verified by the New Jersey Corporation for Advanced Technology (NJCAT) and have been certified by the New Jersey Department of Environmental Protection (NJDEP). Hydroworks, LLC has requested an MTD Laboratory Certification for the Hydroworks HydroStorm Hydrodynamic Separator.

The project falls under the "Procedure for Obtaining Verification of a Stormwater Manufactured Treatment Device from New Jersey Corporation for Advance Technology" dated January 25, 2013. The applicable protocol is the "New Jersey Laboratory Testing Protocol to Assess Total Suspended Solids Removal by a Hydrodynamic Sedimentation Manufactured Treatment Device" dated January 25, 2013.

NJCAT verification documents submitted to the NJDEP indicate that the requirements of the aforementioned protocol have been met or exceeded. The NJCAT letter also included a recommended certification TSS removal rate and the required maintenance plan. The NJCAT Verification Report with the Verification Appendix (dated February 2018) for this device is published online at <a href="http://www.njcat.org/verification-process/technology-verification-database.html">http://www.njcat.org/verification-process/technology-verification-database.html</a>.

The NJDEP certifies the use of the HydroStorm by Hydroworks, LLC at a TSS removal rate of 50% when designed, operated, and maintained in accordance with the information provided in the Verification Appendix and the following conditions:

- 1. The maximum treatment flow rate (MTFR) for the manufactured treatment device (MTD) is calculated using the New Jersey Water Quality Design Storm (1.25 inches in 2 hrs) in N.J.A.C. 7:8-5.5.
- 2. The HydroStorm shall be installed using the same configuration reviewed by NJCAT and shall be sized in accordance with the criteria specified in item 6 below.
- 3. This HydroStorm cannot be used in series with another MTD or a media filter (such as a sand filter) to achieve an enhanced removal rate for total suspended solids (TSS) removal under N.J.A.C. 7:8-5.5.
- 4. Additional design criteria for MTDs can be found in Chapter 9.6 of the New Jersey Stormwater Best Management Practices (NJ Stormwater BMP) Manual, which can be found online at <u>www.njstormwater.org</u>.
- 5. The maintenance plan for a site using this device shall incorporate, at a minimum, the maintenance requirements for the Hydrostorm. A copy of the maintenance plan is attached to this certification. However, it is recommended to review the maintenance website at <a href="http://www.hydroworks.com/hydrostormo&m.pdf">http://www.hydroworks.com/hydrostormo&m.pdf</a> for any changes to the maintenance requirements.
- 6. Sizing Requirement:

The example below demonstrates the sizing procedure for the Hydrostorm:

Example: A 0.25-acre impervious site is to be treated to 50% TSS removal using a HydroStorm. The impervious site runoff (Q) based on the New Jersey Water Quality Design Storm was determined to be 0.79 cfs.

#### Maximum Treatment Flow Rate (MTFR) Evaluation:

The site runoff (Q) was based on the following: time of concentration = 10 minutes i = 3.2 in/hr (page 5-8, Fig. 5-3 of the NJ Stormwater BMP Manual) c = 0.99 (runoff coefficient for impervious) Q = ciA = 0.99 x 3.2 x 0.25 = 0.79 cfs

Given the site runoff is 0.79 cfs and based on Table 1 below, the HydroStorm Model HS4 with a MTFR of 0.88 cfs could be used for this site to remove 50% of the TSS from the impervious area without exceeding the MTFR.

The sizing table corresponding to the available system models is noted below. Additional specifications regarding each model can be found in the Verification Appendix under Table A-1.

HydroStorm Model	NJDEP 50% TSS Maximum Treatment Flow Rate (cfs)	Treatment Area (ft <sup>2</sup> )	Hydraulic Loading Rate (gpm/ft <sup>2</sup> )	50% Maximum Sediment Storage (ft <sup>3</sup> )
HS3	0.50	7.1	31.4	3.6
HS4	0.88	12.6	31.4	6.3
HS5	1.37	19.6	31.4	9.8
HS6	1.98	28.3	31.4	14.2
HS7	2.69	38.5	31.4	19.3
HS8	3.52	50.3	31.4	25.2
HS9	4.45	63.6	31.4	31.8
HS10	5.49	78.5	31.4	39.3
HS11	6.65	95.0	31.4	47.5
HS12	7.91	113.0	31.4	56.5

#### **Table 1 HydroStorm Sizing Information**

A detailed maintenance plan is mandatory for any project with a Stormwater BMP subject to the Stormwater Management Rules, N.J.A.C. 7:8. The plan must include all of the items identified in the Stormwater Management Rules, N.J.A.C. 7:8-5.8. Such items include, but are not limited to, the list of inspection and maintenance equipment and tools, specific corrective and preventative maintenance tasks, indication of problems in the system, and training of maintenance personnel. Additional information can be found in Chapter 8: Maintenance and Retrofit of Stormwater Management Measures.

If you have any questions regarding the above information, please contact Brian Salvo or Nick Grotts of my office at (609) 633-7021.

Sincerely, James J. Murphy, Chief

Bureau of Nonpoint Pollution Control

Attachment: Maintenance Plan

cc: Chron File Richard Magee, NJCAT Vince Mazzei, NJDEP - DLUR Ravi Patraju, NJDEP - BES Gabriel Mahon, NJDEP - BNPC Brian Salvo, NJDEP - BNPC Nick Grotts, NJDEP - BNPC



# Hydroworks® HydroStorm

# **Operations & Maintenance Manual**

Version 1.0

Please call Hydroworks at 888-290-7900 or email us at support@hydroworks.com if you have any questions regarding the Inspection Checklist. Please fax a copy of the completed checklist to Hydroworks at 888-783-7271 for our records.

#### Introduction

The HydroStorm is a state of the art hydrodynamic separator. Hydrodynamic separators remove solids, debris and lighter than water (oil, trash, floating debris) pollutants from stormwater. Hydrodynamic separators and other water quality measures are mandated by regulatory agencies (Town/City, State, Federal Government) to protect storm water quality from pollution generated by urban development (traffic, people) as part of new development permitting requirements.

As storm water treatment structures fill up with pollutants they become less and less effective in removing new pollution. Therefore, it is important that storm water treatment structures be maintained on a regular basis to ensure that they are operating at optimum performance. The HydroStorm is no different in this regard and this manual has been assembled to provide the owner/operator with the necessary information to inspect and coordinate maintenance of their HydroStorm.

#### Hydroworks<sup>®</sup> HydroStorm Operation

The Hydroworks HydroStorm (HS) separator is a unique hydrodynamic by-pass separator. It incorporates a protected submerged pretreatment zone to collect larger solids, a treatment tank to remove finer solids, and a dual set of weirs to create a high flow bypass. High flows are conveyed directly to the outlet and do not enter the treatment area, however, the submerged pretreatment area still allows removal of coarse solids during high flows.

Under normal or low flows, water enters an inlet area with a horizontal grate. The area underneath the grate is submerged with openings to the main treatment area of the separator. Coarse solids fall through the grate and are either trapped in the pretreatment area or conveyed into the main treatment area depending on the flow rate. Fines are transported into the main treatment area. Openings and weirs in the pretreatment area allow entry of water and solids into the main treatment area and cause water to rotate in the main treatment area creating a vortex motion. Water in the main treatment area is forced to rise along the walls of the separator to discharge from the treatment area to the downstream pipe.

The vortex motion forces solids and floatables to the middle of the inner chamber. Floatables are trapped since the inlet to the treatment area is submerged. The design maximizes the retention of settled solids since solids are forced to the center of the inner chamber by the vortex motion of water while water must flow up the walls of the separator to discharge into the downstream pipe.

A set of high flow weirs near the outlet pipe create a high flow bypass over both the pretreatment area and main treatment chamber. The rate of flow into the treatment area is regulated by the number and size of openings into the treatment chamber and the height of by-pass weirs. High flows flow over the weirs directly to the outlet pipe preventing the scour and resuspension of any fines collected in the treatment chamber.



A central access tube is located in the structure to provide access for cleaning. The arrangement of the inlet area and bypass weirs near the outlet pipe facilitate the use of multiple inlet pipes.



Figure 1. Hydroworks HydroStorm Operation – Plan View

Figure 2 is a profile view of the HydroStorm separator showing the flow patterns for low and high flows.





Figure 2. Hydroworks HydroStorm Operation – Profile View

The HS 4i is an inlet version of the HS 4 separator. There is a catch-basin grate on top of the HS 4i. A funnel sits sits underneath the grate on the frame and directs the water to the inlet side of the separator to ensure all lows flows are properly treated. The whole funnel is removed for inspection and cleaning.





Figure 3. Hydroworks HS 4i Funnel

#### Inspection

#### Procedure

#### **Floatables**

A visual inspection can be conducted for floatables by removing the covers and looking down into the center access tube of the separator. Separators with an inlet grate (HS 4i or custom separator) will have a plastic funnel located under the grate that must be removed from the frame prior to inspection or maintenance. If you are missing a funnel please contact Hydroworks at the numbers provided at the end of this document.



#### TSS/Sediment

Inspection for TSS build-up can be conducted using a Sludge Judge®, Core Pro®, AccuSludge® or equivalent sampling device that allows the measurement of the depth of TSS/sediment in the unit. These devices typically have a ball valve at the bottom of the tube that allows water and TSS to flow into the tube when lowering the tube into the unit. Once the unit touches the bottom of the device, it is quickly pulled upward such that the water and TSS in the tube forces the ball valve closed allowing the user to see a full core of water/TSS in the unit. The unit should be inspected for TSS through each of the access covers. Several readings (2 or 3) should be made at each access cover to ensure that an accurate TSS depth measurement is recorded.

#### Frequency

#### **Construction Period**

The HydroStorm separator should be inspected every four weeks and after every large storm (over 0.5" (12.5 mm) of rain) during the construction period.

#### Post-Construction Period

The Hydroworks HydroStorm separator should be inspected during the first year of operation for normal stabilized sites (grassed or paved areas). If the unit is subject to oil spills or runoff from unstabilized (storage piles, exposed soils) areas the HydroStorm separator should be inspected more frequently (4 times per year). The initial annual inspection will indicate the required future frequency of inspection and maintenance if the unit was maintained after the construction period.

#### Reporting

Reports should be prepared as part of each inspection and include the following information:

- 1. Date of inspection
- 2. GPS coordinates of Hydroworks unit
- 3. Time since last rainfall
- 4. Date of last inspection
- 5. Installation deficiencies (missing parts, incorrect installation of parts)
- 6. Structural deficiencies (concrete cracks, broken parts)
- 7. Operational deficiencies (leaks, blockages)
- 8. Presence of oil sheen or depth of oil layer
- 9. Estimate of depth/volume of floatables (trash, leaves) captured
- 10. Sediment depth measured
- 11. Recommendations for any repairs and/or maintenance for the unit
- 12. Estimation of time before maintenance is required if not required at time of inspection



A sample inspection checklist is provided at the end of this manual.

#### **Maintenance**

#### Procedure

The Hydroworks HydroStorm unit is typically maintained using a vacuum truck. There are numerous companies that can maintain the HydroStorm separator. Maintenance with a vacuum truck involves removing all of the water and sediment together. The water is then separated from the sediment on the truck or at the disposal facility.

A central access opening (24" or greater) is provided to the gain access to the lower treatment tank of the unit. This is the primary location to maintain by vacuum truck. The pretreatment area can also be vacuumed and/or flushed into the lower treatment tank of the separator for cleaning via the central access once the water level is lowered below the pretreatment floor.

In instances where a vacuum truck is not available other maintenance methods (i.e. clamshell bucket) can be used, but they will be less effective. If a clamshell bucket is used the water must be decanted prior to cleaning since the sediment is under water and typically fine in nature. Disposal of the water will depend on local requirements. Disposal options for the decanted water may include:

- 1. Discharge into a nearby sanitary sewer manhole
- 2. Discharge into a nearby LID practice (grassed swale, bioretention)
- 3. Discharge through a filter bag into a downstream storm drain connection

The local municipality should be consulted for the allowable disposal options for both water and sediments prior to any maintenance operation. Once the water is decanted the sediment can be removed with the clamshell bucket.

Disposal of the contents of the separator depend on local requirements. Maintenance of a Hydroworks HydroStorm unit will typically take 1 to 2 hours based on a vacuum truck and longer for other cleaning methods (i.e. clamshell bucket).





Figure 3. Maintenance Access

#### Frequency

#### Construction Period

A HydroStorm separator can fill with construction sediment quickly during the construction period. The HydroStorm must be maintained during the construction period when the depth of TSS/sediment reaches 24" (600 mm). It must also be maintained during the construction period if there is an appreciable depth of oil in the unit (more than a sheen) or if floatables other than oil cover over 50% of the area of the separator

The HydroStorm separator should be maintained at the end of the construction period, prior to operation for the post-construction period.



#### Post-Construction Period

The HydroStorm was independently tested by Alden Research Laboratory in 2017. A HydroStorm HS 4 was tested for scour with a 50% sediment depth of 0.5 ft. Therefore, maintenance for sediment accumulation is required if the depth of sediment is 1 ft or greater in separators with standard water (sump) depths (Table 1).

There will be designs with increased sediment storage based on specifications or site-specific criteria. A measurement of the total water depth in the separator through the central access tube should be taken and compared to water depth given in Table 1. The standard water depth from Table 1 should be subtracted from the measured water depth and the resulting extra depth should be added to the 1 ft to determine the site-specific sediment maintenance depth for that separator.

For example, if the measured water depth in the HS-7 is 7 feet, then the sediment maintenance depth for that HS-7 is 2 ft (= 1 + 7 - 6) and the separator does not need to be cleaned for sediment accumulation until the measure sediment depth is 2 ft.

The HydroStorm separator must also be maintained if there is an appreciable depth of oil in the unit (more than a sheen) or if floatables other than oil cover over 50% of the water surface of the separator.

Model	Diameter (ft)	Total Water Depth (ft)	Sediment Maintenance Depth for Table 1 Total Water Depth(ft)
HS-3	3	3	1
HS-4	4	4	1
HS-5	5	4	1
HS-6	6	4	1
HS-7	7	6	1
HS-8	8	7	1
HS-9	9	7.5	1
HS-10	10	8	1
HS-11	11	9	1
HS-12	12	9.5	1

 Table 1 Standard Dimensions for Hydroworks HydroStorm Models



## HYDROSTORM INSPECTION SHEET

Date Date of Last Inspection			
Site City State Owner			
GPS Coordinates			
Date of last rainfall			
Site Characteristics Soil erosion evident Exposed material storage Large exposure to leaf little High traffic (vehicle) area	on site er (lots of trees)	Yes	No       
HydroStorm Obstructions in the inlet or Missing internal component Improperly installed inlet of Internal component damage Floating debris in the sepa Large debris visible in the Concrete cracks/deficience Exposed rebar Water seepage (water level Water level depth be	outlet hts r outlet pipes ge (cracked, broken, loose pieces) irator (oil, leaves, trash) separator es not at outlet pipe invert) low outlet pipe invert	Yes	No 
Routine Measurements Floating debris depth Floating debris coverage Sludge depth	< 0.5" (13mm)	>0.5" 13mm) > 50% surface are > 12" (300mm)	□ * a □ * □ *

- \*
- \*\*
- Maintenance required Repairs required Further investigation is required \*\*\*



Other Comments:	
	Hydroworks



## Hydroworks<sup>®</sup> HydroStorm

### One Year Limited Warranty

Hydroworks, LLC warrants, to the purchaser and subsequent owner(s) during the warranty period subject to the terms and conditions hereof, the Hydroworks HydroStorm to be free from defects in material and workmanship under normal use and service, when properly installed, used, inspected and maintained in accordance with Hydroworks written instructions, for the period of the warranty. The standard warranty period is 1 year.

The warranty period begins once the separator has been manufactured and is available for delivery. Any components determined to be defective, either by failure or by inspection, in material and workmanship will be repaired, replaced or remanufactured at Hydroworks' option provided, however, that by doing so Hydroworks, LLC will not be obligated to replace an entire insert or concrete section, or the complete unit. This warranty does not cover shipping charges, damages, labor, any costs incurred to obtain access to the unit, any costs to repair/replace any surface treatment/cover after repair/replacement, or other charges that may occur due to product failure, repair or replacement.

This warranty does not apply to any material that has been disassembled or modified without prior approval of Hydroworks, LLC, that has been subjected to misuse, misapplication, neglect, alteration, accident or act of God, or that has not been installed, inspected, operated or maintained in accordance with Hydroworks, LLC instructions and is in lieu of all other warranties expressed or implied. Hydroworks, LLC does not authorize any representative or other person to expand or otherwise modify this limited warranty.

The owner shall provide Hydroworks, LLC with written notice of any alleged defect in material or workmanship including a detailed description of the alleged defect upon discovery of the defect. Hydroworks, LLC should be contacted at 136 Central Ave., Clark, NJ 07066 or any other address as supplied by Hydroworks, LLC. (888-290-7900).

This limited warranty is exclusive. There are no other warranties, express or implied, or merchantability or fitness for a particular purpose and none shall be created whether under the uniform commercial code, custom or usage in the industry or the course of dealings between the parties. Hydroworks, LLC will replace any goods that are defective under this warranty as the sole and exclusive remedy for breach of this warranty.

Subject to the foregoing, all conditions, warranties, terms, undertakings or liabilities (including liability as to negligence), expressed or implied, and howsoever arising, as to the condition, suitability, fitness, safety, or title to the Hydroworks HydroStorm are hereby negated and excluded and Hydroworks, LLC gives and makes no such representation, warranty or undertaking except as expressly set forth herein. Under no circumstances shall Hydroworks, LLC be liable to the Purchaser or to any third party for product liability claims; claims arising from the design, shipment, or installation of the HydroStorm, or the cost of other goods or services related to the purchase and installation of the HydroStorm. For this Limited Warranty to apply, the HydroStorm must be installed in accordance with all site conditions required by state and local codes; all other applicable laws; and Hydroworks' written installation instructions.

Hydroworks, LLC expressly disclaims liability for special, consequential or incidental damages (even if it has been advised of the possibility of the same) or breach of expressed or implied warranty. Hydroworks, LLC shall not be liable for penalties or liquidated damages, including loss of production and profits; labor and materials; overhead costs; or other loss or expense incurred by the purchaser or any third party. Specifically excluded from limited warranty coverage are damages to the HydroStorm arising from ordinary wear and tear; alteration, accident, misuse, abuse or neglect; improper maintenance, failure of the product due to improper installation of the concrete sections or improper sizing; or any other event not caused by Hydroworks, LLC. This limited warranty represents Hydroworks' sole liability to the purchaser for claims related to the HydroStorm, whether the claim is based upon contract, tort, or other legal basis.

FIGURES





<u>SOILS LEGEND</u>		
DESCRIPTION	HYDROLOGICAL GROUP	
Silt Loam, 3% to 8% slope	C/D	
Silt Loam, 8% to 15% slope	C/D	
a Silt Loam, Nuetral Substratum	C/D	
digan Complex, Rolling, Very Rocky	D	
NRCS Soil Boundary Line		

<u>LEG</u>	END
	SUBCATCHMENT
$\rightarrow$	TIME OF CONCENTRATION SHEET FLOW
$\rightarrow$	TIME OF CONCENTRATION SHALLOW CONCENTRATED FLOW
	DESIGN LINE
//. /.	SUBCATCHMENT CONTRIBUTING AREA

REVISION		BY
<b>S / T E</b> ERING, SURVEYING & PE ARCHITECTURE, P.C.	3 Garrett Place Carmel, NY 10512 (845) 225–9690 (845) 225–9717 fo www.insite–eng.con	אב ז
<u>V VIEWS</u> HESS COUNTY, NEW YORK <u>ELOPMENT</u> <u>GE MAP</u>		
PROJECT J. J. C.	FIGURE NO.	
DRAWN BY E.J.P.	2	
CHECKED Z.M.P.		



<u>SOILS LEGEND</u>		
DESCRIPTION	HYDROLOGICAL GROUP	
Silt Loam, 3% to 8% slope	C/D	
Silt Loam, 8% to 15% slope	C/D	
a Silt Loam, Nuetral Substratum	C/D	
digan Complex, Rolling, Very Rocky	D	
NRCS Soil Boundary Line		

<u>LEGEND</u>	
	SUBCATCHMENT
7	STORMWATER MANAGEMENT PRACTICE
$\rightarrow$	TIME OF CONCENTRATION SHEET FLOW
$\rightarrow$	TIME OF CONCENTRATION SHALLOW CONCENTRATED FLOW
$\rightarrow$	TIME OF CONCENTRATION PIPE FLOW
$\rightarrow$	TIME OF CONCENTRATION CHANNEL FLOW
	DESIGN LINE
	SUBCATCHMENT CONTRIBUTING AREA
	STORMWATER MANAGEMENT PRACTICE AREA

REVISION			BY
<b>S / T</b> ERING, SURVEY PE ARCHITECTUR	<b>E</b> ING & RE, P.C.	3 Garrett Place Carmel, NY 10512 (845) 225–9690 (845) 225–9717 fo www.insite–eng.con	ax n
<u>V VIEWS</u> hess county, new york <u>(ELOPMENT</u> <u>GE MAP</u>			
PROJECT MANAGER	J. J. C.	FIGURE NO.	
DRAWN BY	<i>E.J.P</i> .	.3	
CHECKED BY	Z.M.P.	)	